

# Compact Model of Single TeraFET Spectrometer



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**11<sup>th</sup> International MOS-AK Workshop  
(co-located with the IEDM and CMC Meetings)  
Silicon Valley, December 5, 2018**

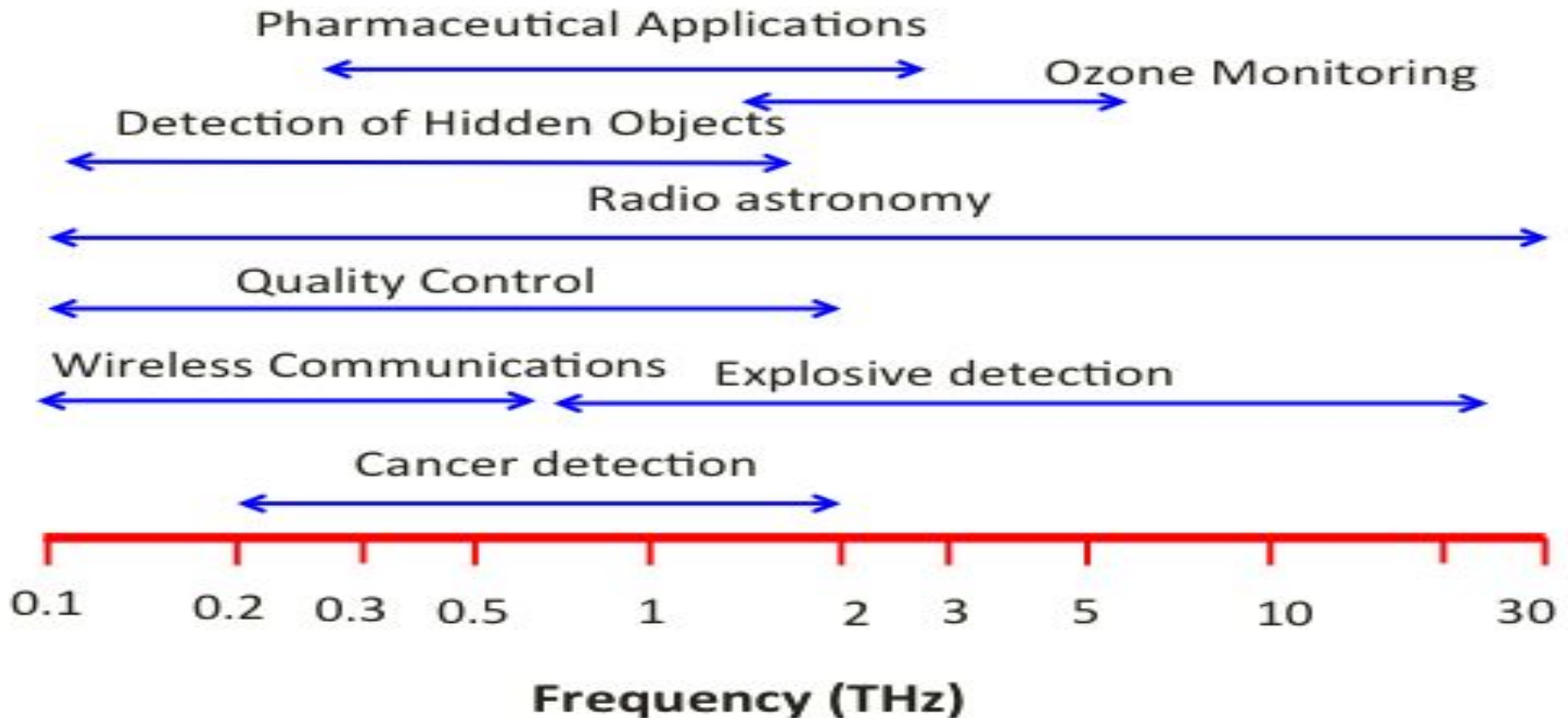
# Outline

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- **Motivation**
- **Plasmonic Detectors Controlled by Phase Asymmetry → resonant TeraFETs**
  - **Basic Equations**
  - **Results and Discussion**
- **Conclusions**

# THz Ranges and Applications

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**Si and SiGe range**

# From 1G to Beyond 5G WIFI

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- 1G            0.8 GHz
- 3G            1.8 to 2.5 GHz
- 4G            2 to 8 GHz        (2012-2018)
- 5G            1 to 28 GHz        (2019-2020)
- Beyond 5G    1 to 1,000 GHz    (2020-2025)

**How could FET technology  
support Beyond 5G?**

**SAMSUNG ,TSMC, Global foundry 7 nm:  
20-30 percent higher performance, 30-50 percent less  
power, 40% shrink compared to 10 nm**

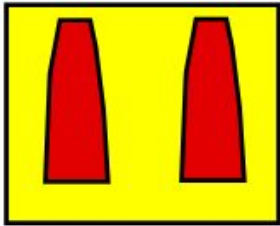
5

- **SAMSUNG 7 nm 27 nm fin pitch 54 nm gate pitch**
  - **256Mb SRAM test chips and application processor (six-core GPU)**
- **TSMC 7nm**
  - **Mobile and network processors, CPUs, graphics processors, FPGAs, and AI accelerators**
- **Gate All Around 3 nm**

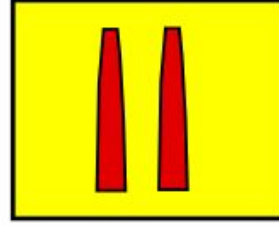
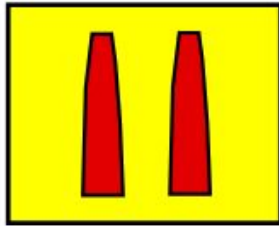
# 22, 14, 10, 7 nm, 3nm Gate All around planned

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**22 nm  
FIN technology**



**10 nm  
FIN technology**



**14 nm  
FIN technology**

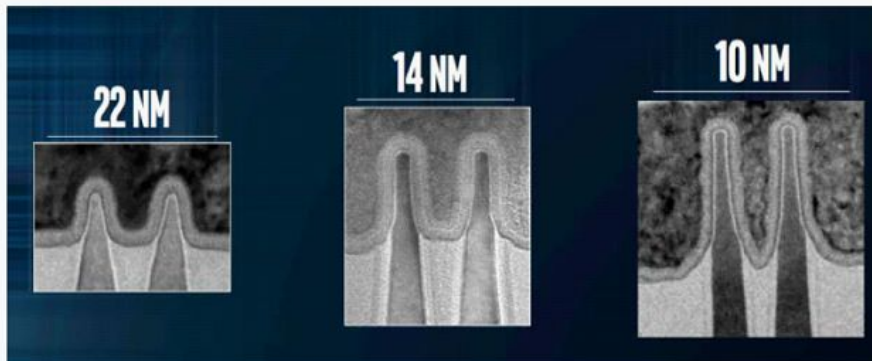


Image: Intel

# DARPA Electronics Resurgence Initiative

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- The U.S. Defense Advanced Research Projects Agency is launching a huge expansion of its Electronics Resurgence Initiative, boosting the program to US \$1.5 billion over five years.
- One of the thrusts is stated as " What can you do with older manufacturing nodes (like 90 nanometers) to make them competitive with 5-nm or 7-nm design?"

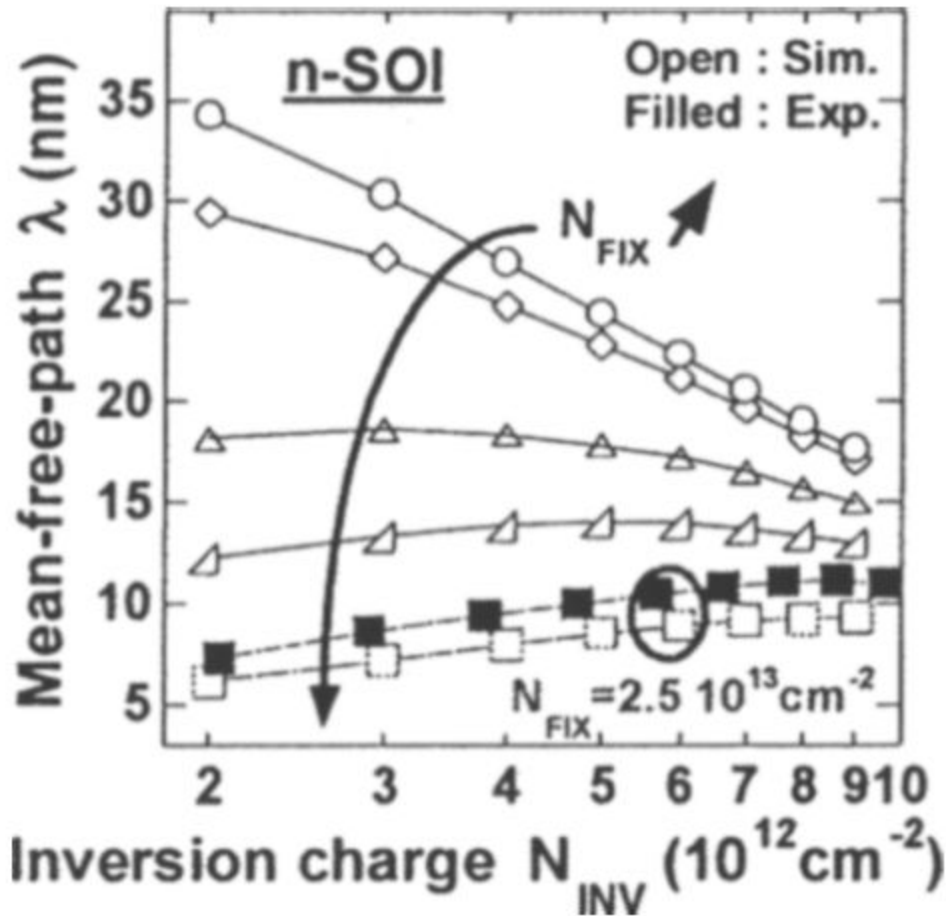
# Ballistic and quasi-ballistic transport in Si

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**Even longer channel  
Si CMOS and Si/SiGe  
BiCMOS operate in  
THz range?**



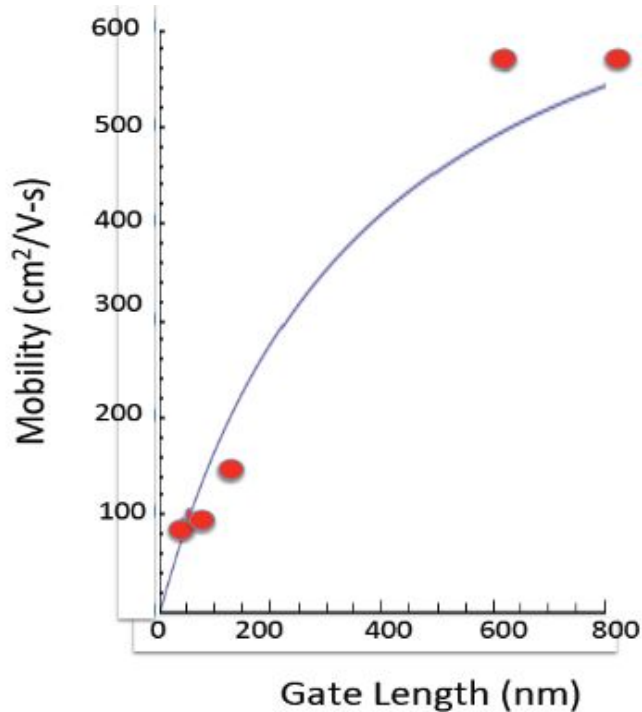
# Mean Free Path in Silicon Inversion Layers



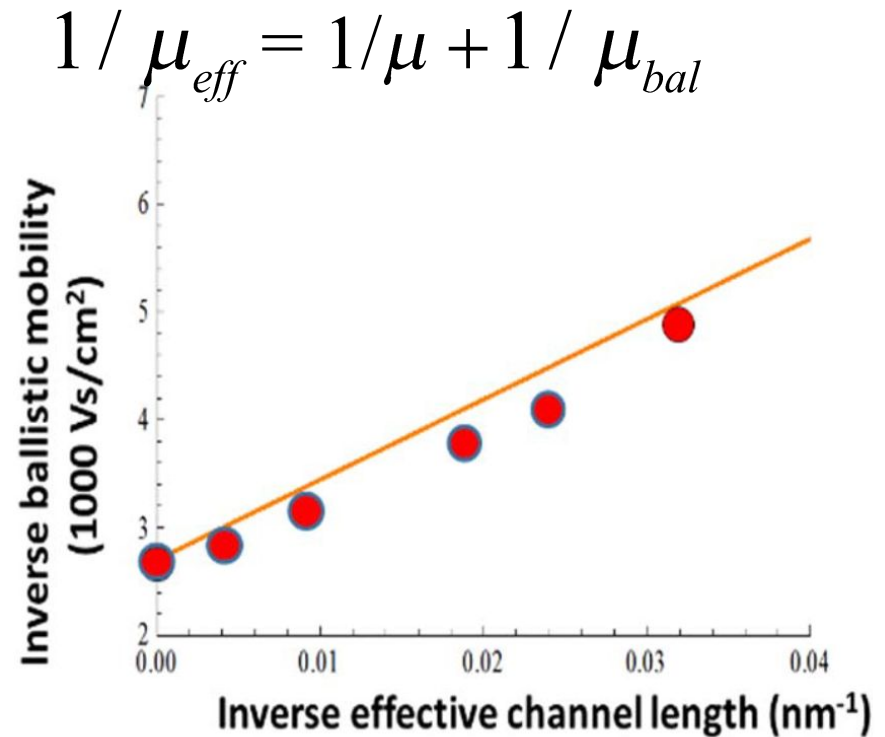
v. Barral'r', T. Poiroux', S. Barraud', O. Bonne', F. Andrieu', C. Buj-Dufournet', L. Brevard', D. Lafond', O. Faynot', D. Munteanu', J.L. Auarr' and S. Deleonibus, Electron Mean-Free-Path Experimental Extraction on Ultra-Thin and Ultra-Short Strained and Unstrained FDSOI n-MOSFETs  
[ieeexplore.ieee.org/iel5/5406683/5418382/05418445.pdf](http://ieeexplore.ieee.org/iel5/5406683/5418382/05418445.pdf)

# Ballistic mobility in Si: proportional to length (A. Kastalski and M. Shur, 1981)

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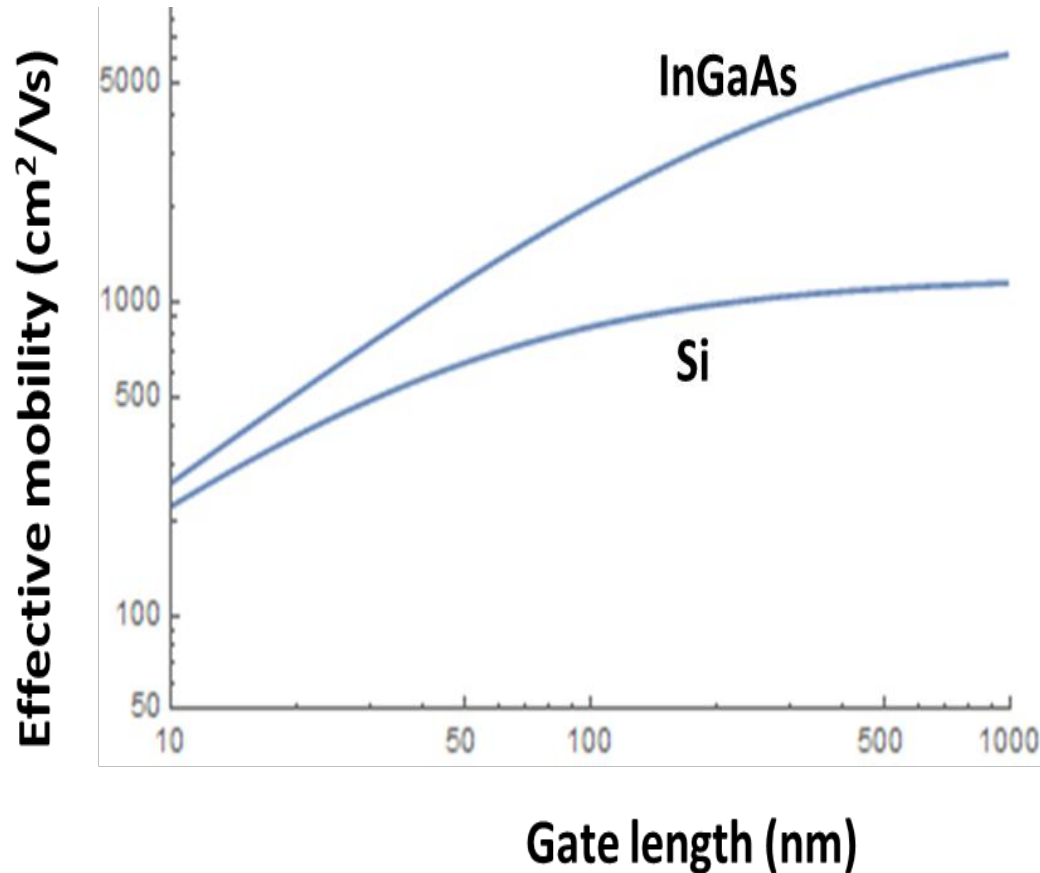
Data from W. Knap, F. Teppe, Y. Meziani, N. Dyakonova, J. Lusakowski, F. Bouef, T. Skotnicki, D. Maude, S. Romyantsev and M. S. Shur, Appl. Phys. Lett, Vol. 85, No 4, pp. 675-677 (2004)



D. Antoniadis, IEEE Transactions on Electron Dev. Vol. 63, No 7, pp. 2650 – 2656 (2016)

# Effective mobility for InGaAs and Si versus gate length

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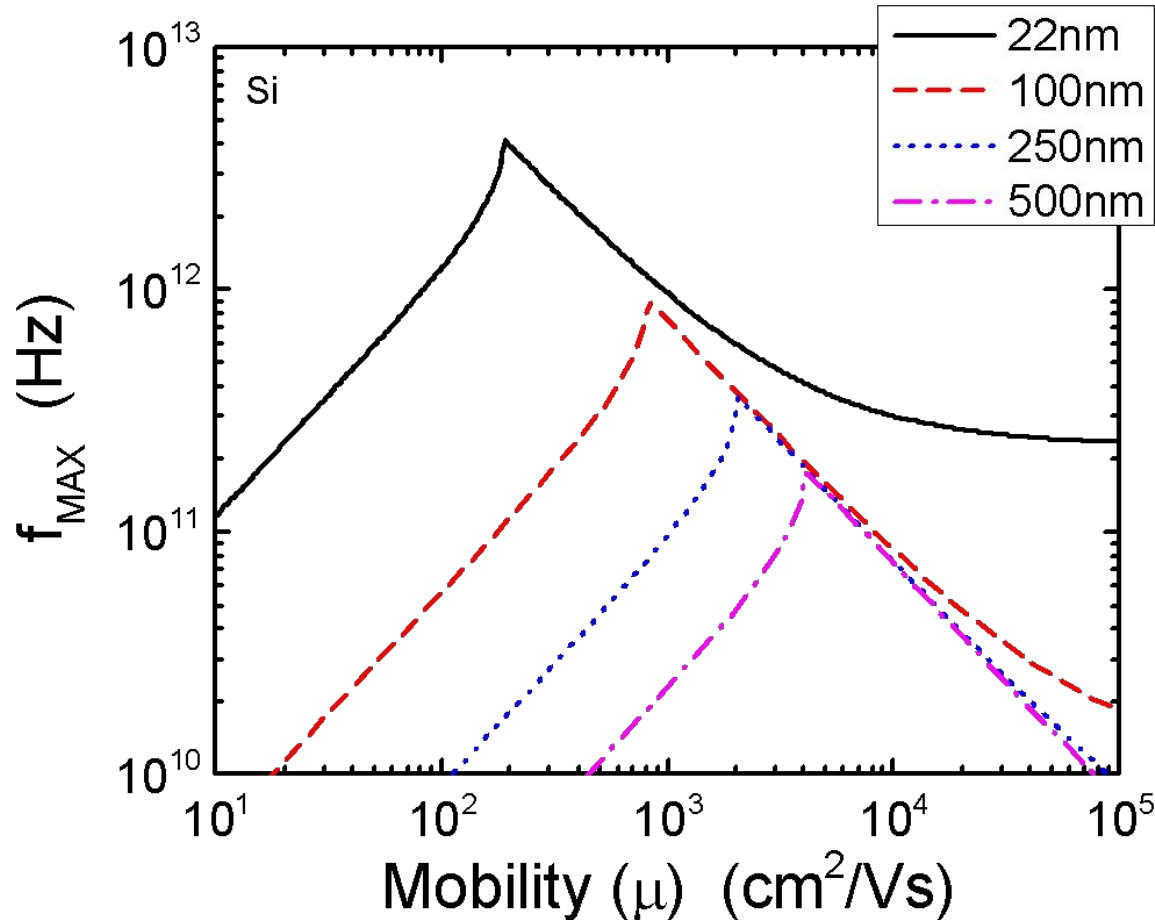


Parameters used in the calculation: the silicon effective mass 0.19; InGaAs effective mass 0.041,  $n_s = 2 \times 10^{16} \text{ m}^{-2}$ , room temperature electron mobility 1200 cm<sup>2</sup>/Vs and 8500 cm<sup>2</sup>/Vs for Si and InGaAs, respectively.

# Maximum Modulation Frequency of Si MOS

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**i S**



“Response of Plasmonic Terahertz Detectors to Amplitude Modulated Signals”,  
Solid-State Electronics 111, Pages 76-79; G. Rupper, S. Rudin, and M. Shur.

# Response of field effect transistor and plasma crystal to the THz radiation

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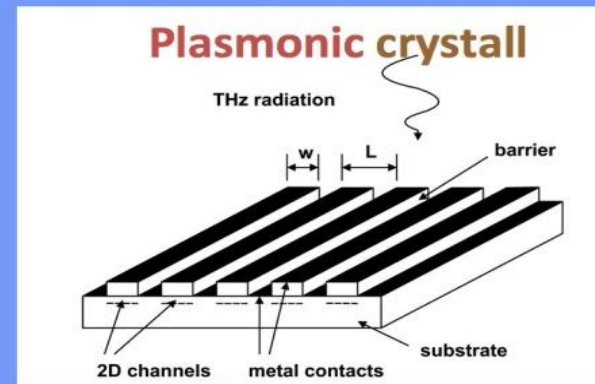
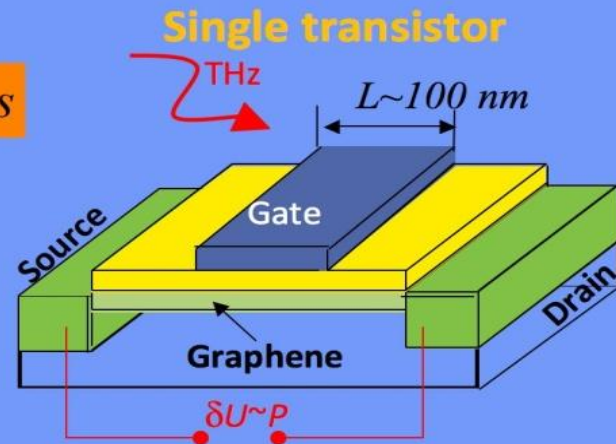
## Plasma wave terahertz electronics

Plasma waves can propagate much faster than electrons:  $s \sim 10^8 \text{ cm / s}$

Channel of FET plays a role of a resonant cavity for plasma waves. Resonant frequency can be tuned by gate voltage:  $\omega_0 = \pi s / 2L \propto \sqrt{U_g}$

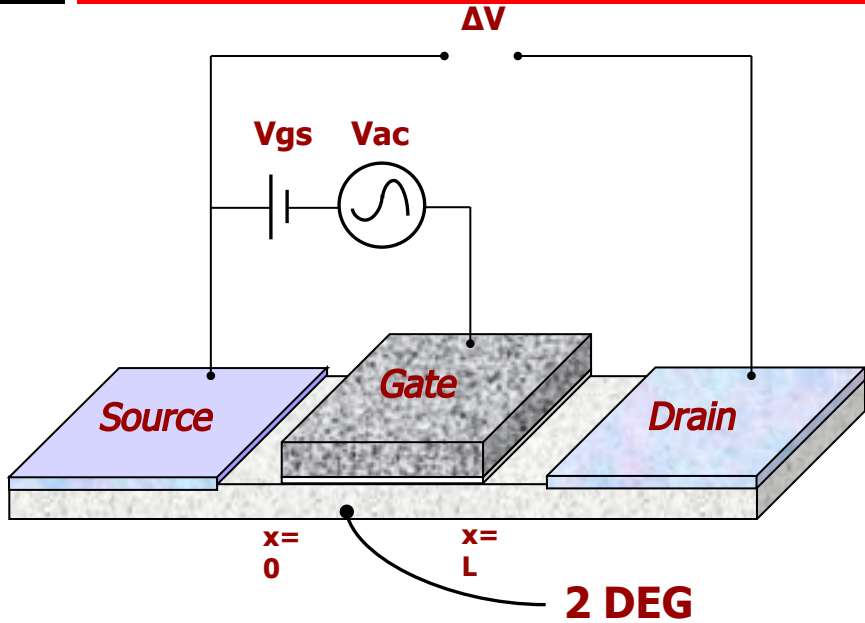
Nonlinearity of plasma waves can be used for **THz detection**. Response is proportional to radiation power:  $\delta U \propto P$

Dc current in the channel excites plasma waves  $\rightarrow$  **THz emission**



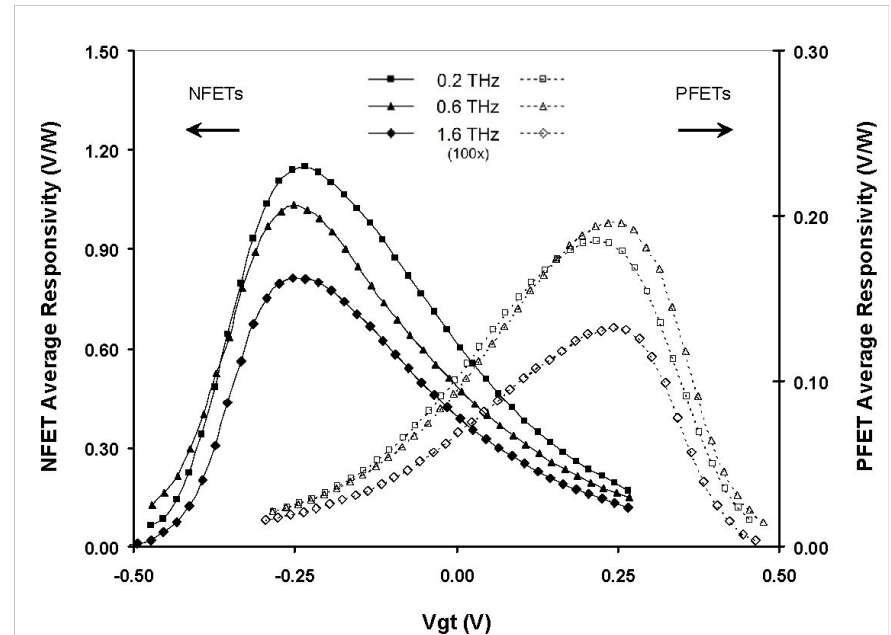
# Rectification of plasma waves enables THz detection

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Conceptual schematic of FET terahertz response.  $V_{ac}$  is the induced voltage resulting from the incident beam;  $\Delta V$  is the proportional drain voltage response.

After: M. Dyakonov and M. Shur, "Detection, mixing, and frequency multiplication of terahertz radiation by two-dimensional electronic fluid," *IEEE Transactions on Electron Devices*, vol. 43, pp. 380-387, 1996.

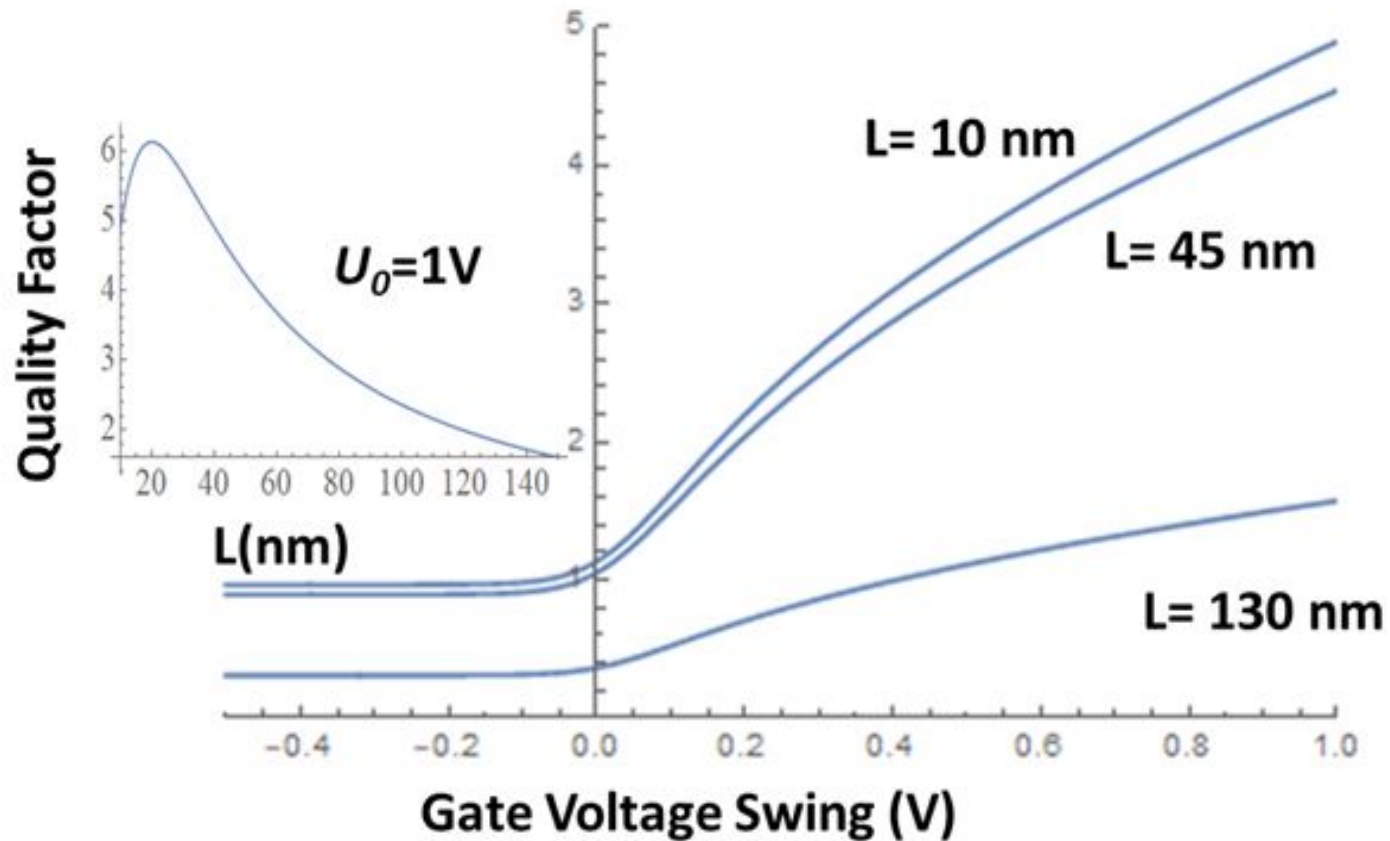


Averaged response of  $2 \mu\text{m}$  width NFETs and  $5 \mu\text{m}$  PFETs at 0.2, 0.6 and 1.6 THz illustrating broad range complementary behavior.

Source: W. Stillman, F. Guarin, V. Y. Kachorovskii, N. Pala, S. Romyantsev, M. S. Shur, and D. Veksler, "Nanometer scale complementary silicon MOSFETs as detectors of terahertz and sub-terahertz radiation," Atlanta, GA, USA, 2007.

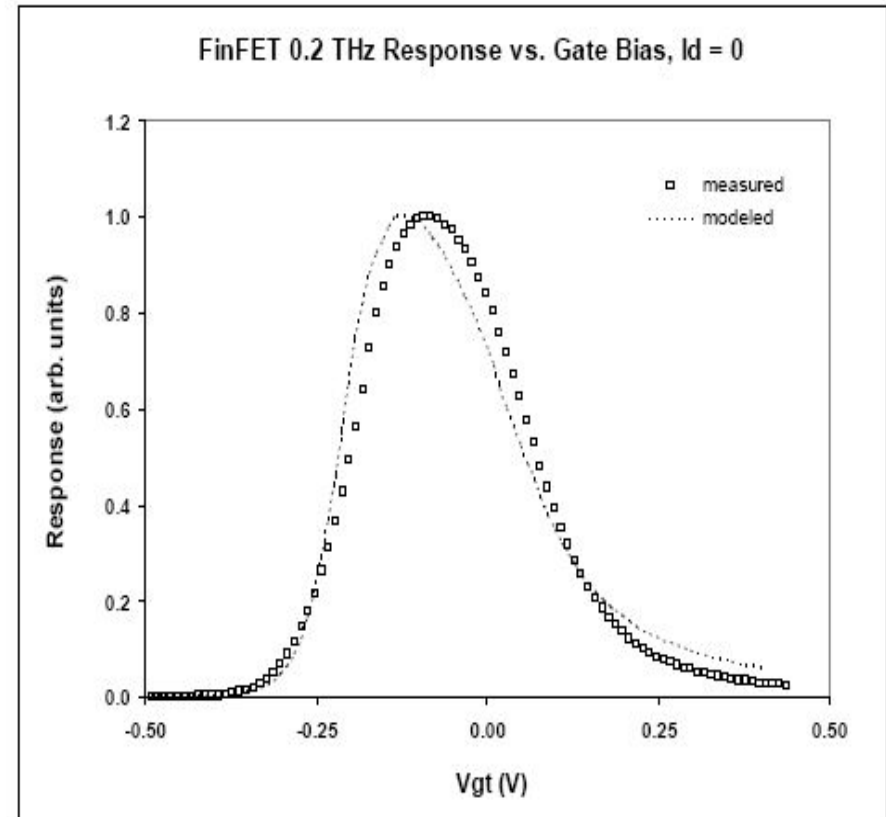
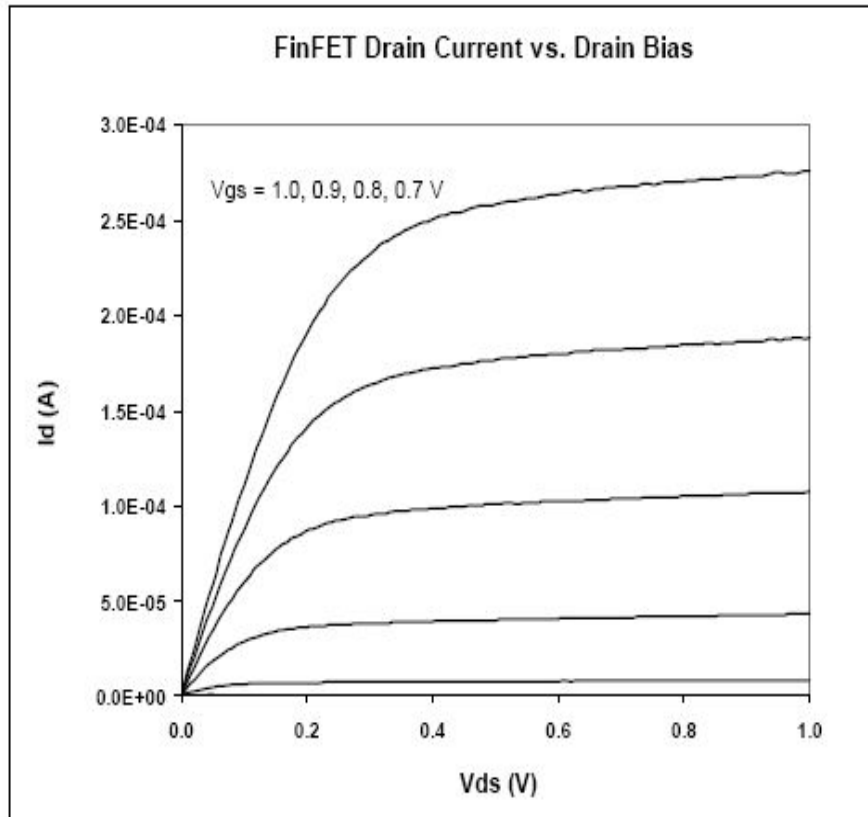
# Quality factors for gated Si MOS region

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# FinFET Response to 0.2 THz

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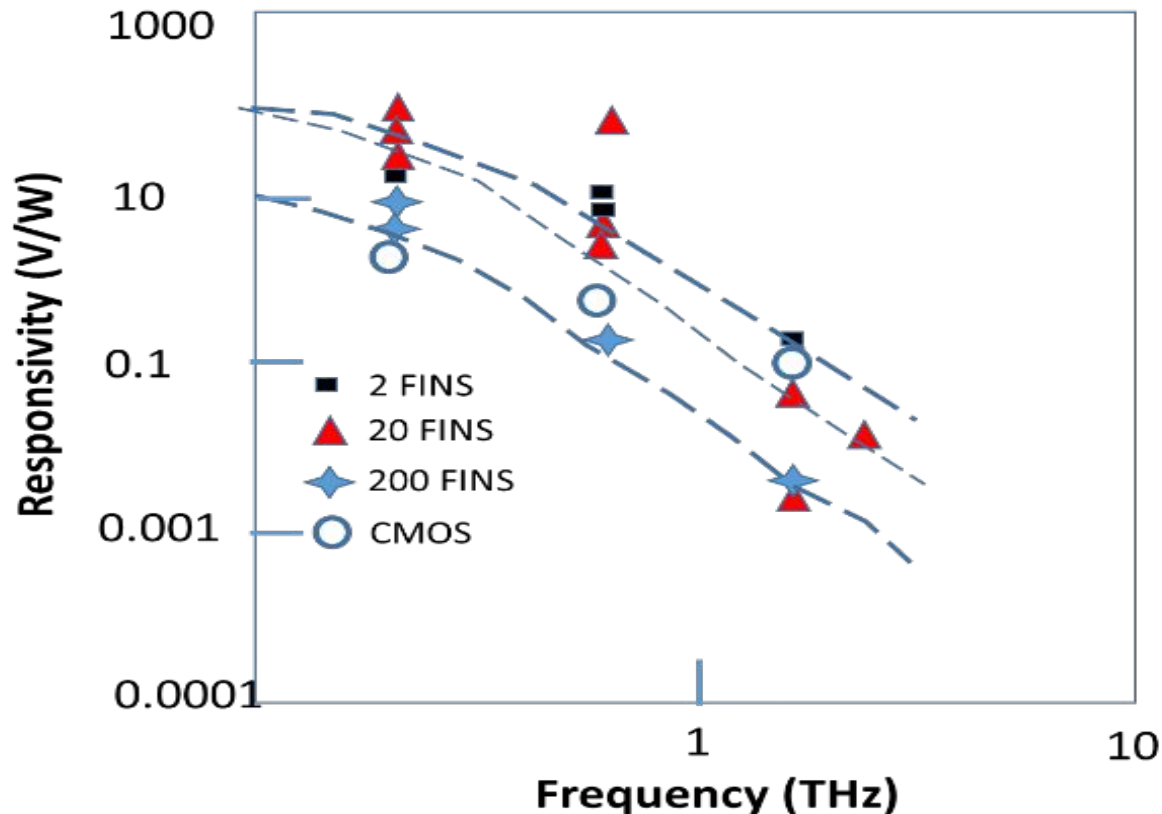


W. Stillman, C. Donais, S. Romyantsev, M. Shur, D. Veksler, C. Hobbs, C. Smith, G. Bersuker, W. Taylor and R. Jammy, Silicon FIN FETs as detectors of terahertz and sub-terahertz radiation, *International Journal of High Speed Electronics and Systems*, vol. 20, No. 1, pp. 27-42 March (2011)



# Silicon CMOS Plasmonic detectors work up to 5 THz

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After W. Stillman, C. Donais, S. Romyantsev, M. Shur, D. Veksler, C. Hobbs, C. Smith, G. Bersuker,

W. Taylor and R. Jammy, Silicon FIN FETs as detectors of terahertz and sub-terahertz radiation,

International Journal of High Speed Electronics and Systems, vol. 20, No. 1, pp. 27-42 March

**THz compact model  
is required for THz  
design**

# *AIM-Spice new models*

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- ❑ HBT
- ❑ MOSFET and SOI (5 new models , *n*- and *p*-channel)
- ❑ MESFET (2 new models)
- ❑ HFET model
- ❑ a-Si TFT and poly TFT models
- ❑ THz HFET and CMOS (under development)
- ❑ TeraFET Spectrometer – THIS WORK

# Unified Charge Control Model

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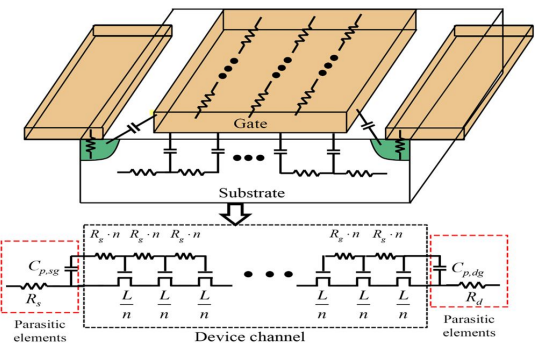
$$n_s = n_o \ln \left[ 1 + \exp \left( \frac{V_{GT} - \alpha V_F}{\eta V_{th}} \right) \right]$$

where the carrier sheet density at threshold is given by

$$n_o = \frac{\eta V_{th} c_i}{q}$$

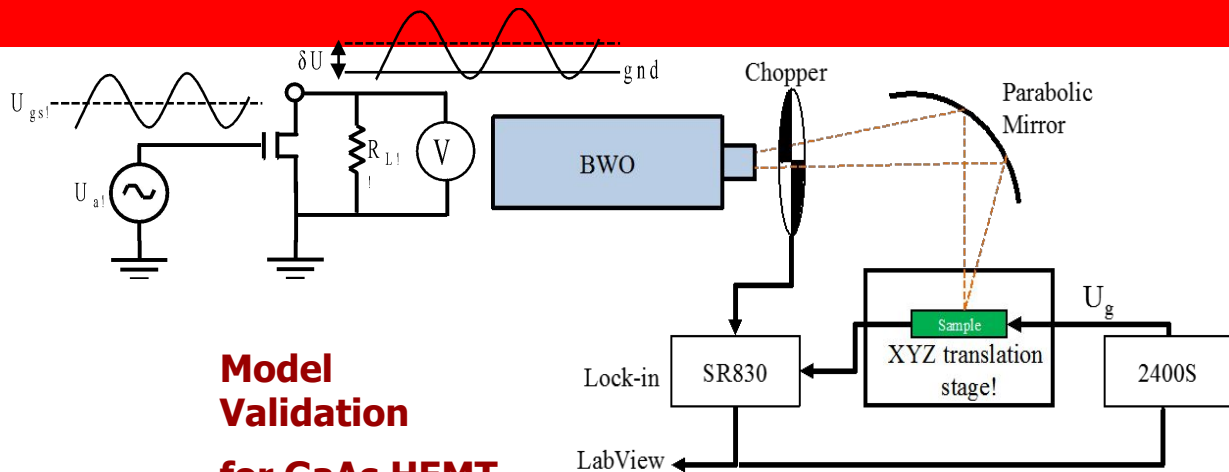
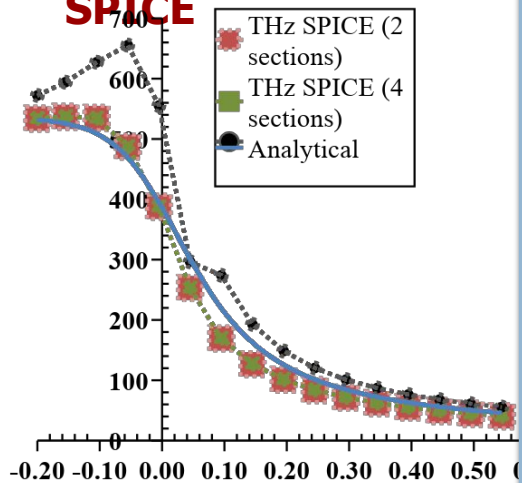
(After T. A. Fjeldly, T. Ytterdal, and M. S. Shur  
Introduction to Device Modeling and Circuit Simulation,  
Wiley, New York (1998), Section 6.3)

# THz SPICE



**THz SPICE  
versus**

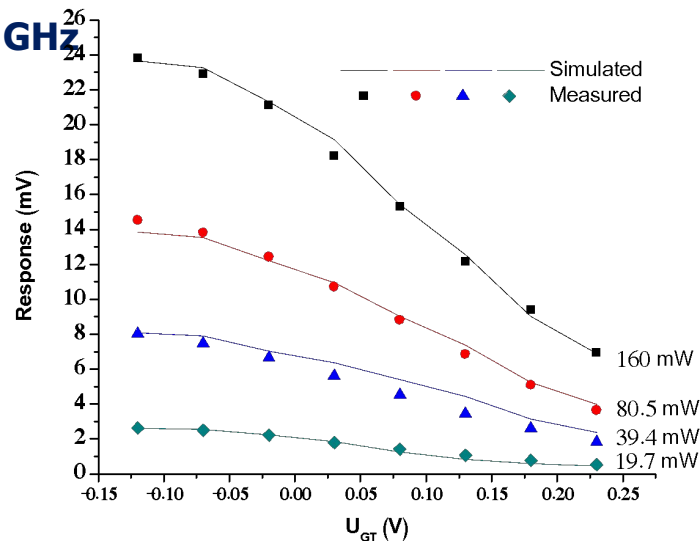
**Traditional  
SPICE**



**Model  
Validation**

**for GaAs HEMT**

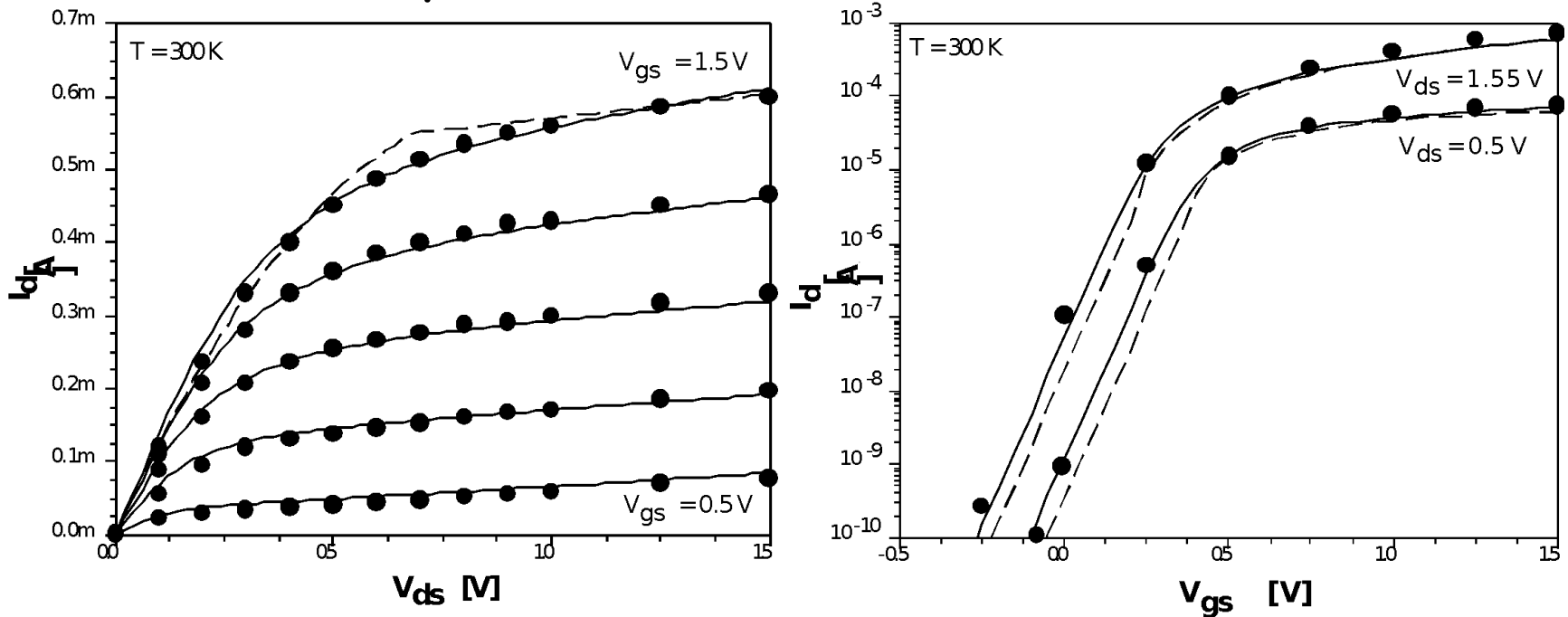
**Simulated Si NMOS  
response for at 200 GHz**



# AIM-SPICE MOSFET model

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IBM Sub-0.1  $\mu\text{m}$  process,  $L_{\text{eff}} = 0.09$   
 $\mu\text{m}$



Simulated (solid lines) and measured (dots) I-V characteristics. The dashed

lines are simulated characteristics using the SPICE MOSFET level 3 model

# Rectification of plasma waves requires asymmetry between source and drain

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Radiation amplitude  $U_a$  is fixed at source, current fixed at drain

$$V_{dc} \propto U_a^2$$

Radiation amplitudes  $U_a$  and  $U_b$  fixed at source and drain

$$V_{dc} \propto U_a^2 - U_b^2$$

Radiation has equal amplitudes at source and drain but phase-shifted by  $\theta$

$$V_{dc} \propto U_a^2 \sin \theta$$

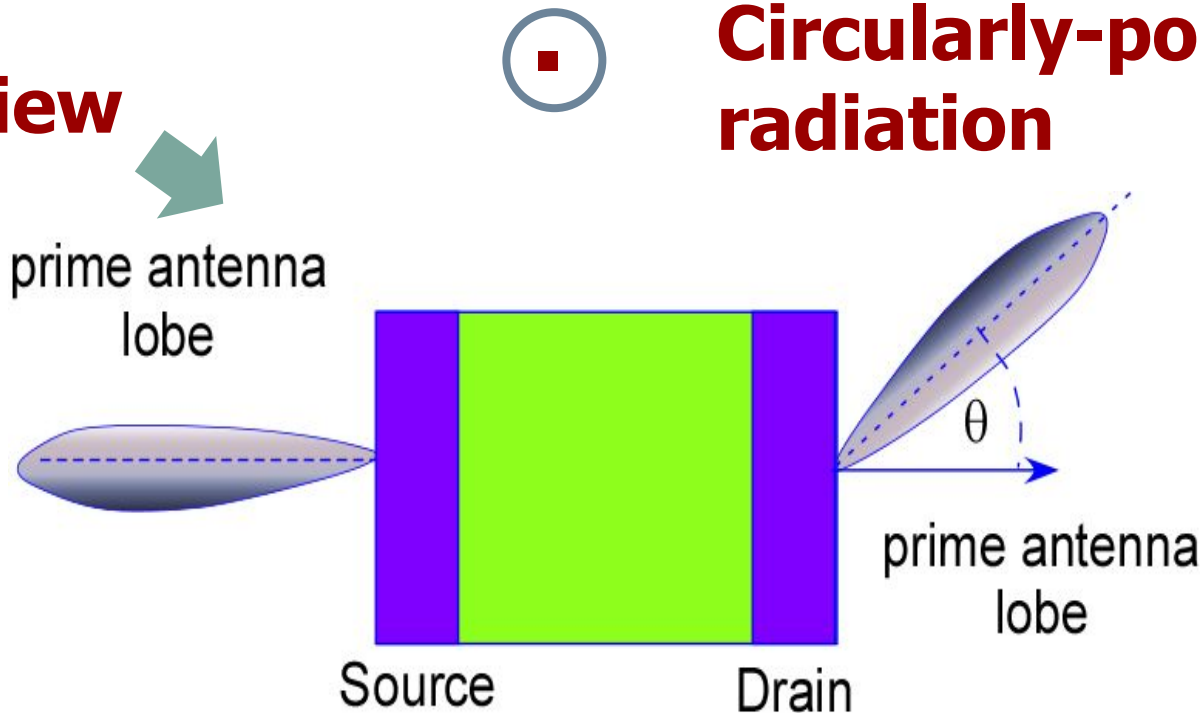


**phase-sensitive spectroscopy**

# Plasmonic Detectors Controlled by Phase Asymmetry → resonant TeraFETs

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**Top view**



**Circularly-polarized radiation**

**Phase Asymmetry imposed by BC**

$$U(0) = U_g + U_a \cos(\omega t + \theta),$$

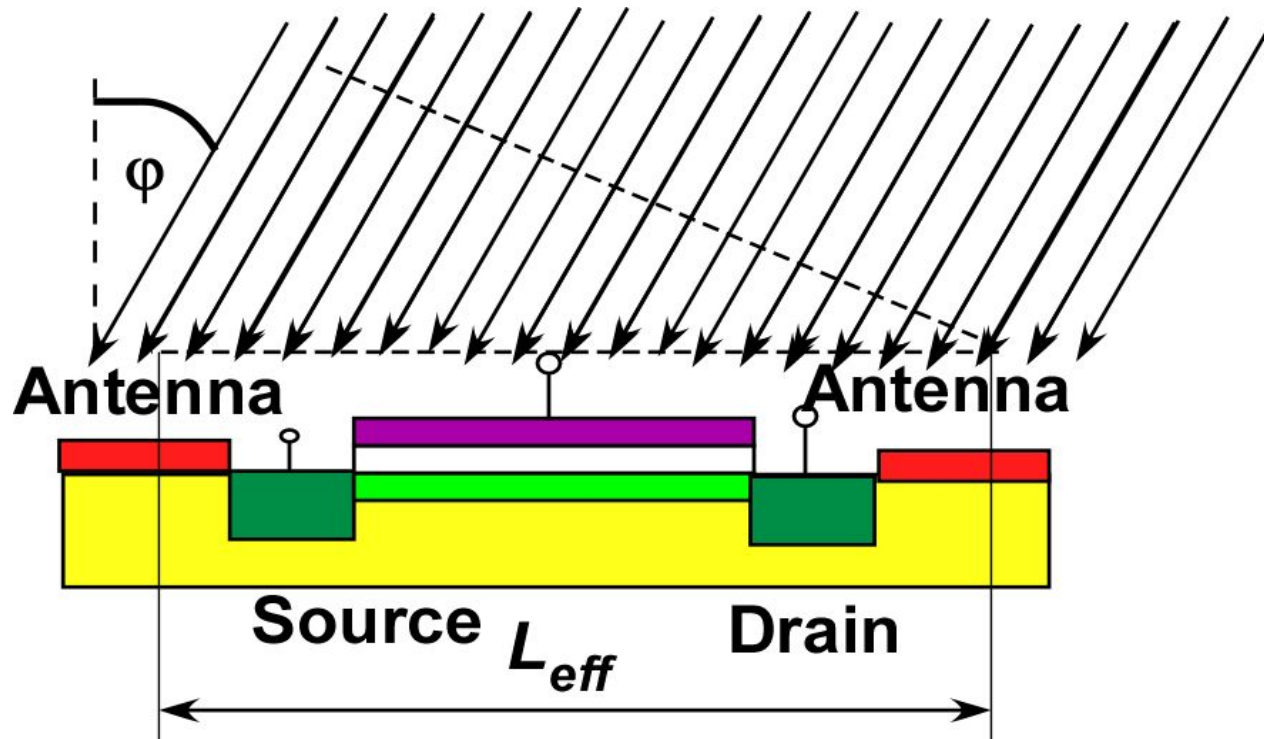
$$U(L) = U_g + V + U_b \cos(\omega t).$$

**direction of  
dc current  
is determined  
by phase shift**



# Phase Asymmetry induced by nonzero incident angle of incoming radiation

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# Hydrodynamics of plasma waves

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$$\begin{cases} \frac{\partial v}{\partial t} + v \frac{\partial v}{\partial x} + \gamma v = -\frac{e}{m} \frac{\partial U}{\partial x}, \\ \frac{\partial U}{\partial t} + \frac{\partial(Uv)}{\partial x} = 0. \end{cases}$$

**Navier-Stokes equation**

**Continuity equation**

$$n(x) = \frac{CU(x)}{e}$$

**Gradual channel approximation**

$$\begin{aligned} U(0) &= U_g + U_a \cos(\omega t + \theta), \\ U(L) &= U_g + V + U_b \cos(\omega t). \end{aligned}$$

**Boundary conditions**

# Rectification of plasma waves

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$$\begin{cases} \frac{\partial v}{\partial t} + v \frac{\partial v}{\partial x} + \gamma v = -\frac{e}{m} \frac{\partial U}{\partial x}, \\ \frac{\partial U}{\partial t} + \frac{\partial(Uv)}{\partial x} = 0. \end{cases} \quad \text{nonlinear terms}$$

$$n = n_0(x) + [n_1(x)e^{-i\omega t} + n_{-1}(x)e^{i\omega t}]/2 + \dots,$$
$$v = v_0(x) + [v_1(x)e^{-i\omega t} + v_{-1}(x)e^{i\omega t}]/2 + \dots$$

 **rectification**

$$\frac{V_{dc}}{U_g} = \frac{\gamma}{4s^2} \int_0^L dx \left( n_1 v_{-1} + n_{-1} v_1 - \frac{d[v_1(x)v_{-1}(x)]}{\gamma dx} \right)$$

# Final result

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$$V = \frac{\omega}{\sqrt{\omega^2 + \gamma^2}} \frac{\alpha(U_a^2 - U_b^2) + \beta U_a U_b \sin\theta}{4U_g |\sin(kL)|^2}$$

$$\alpha = \left(1 + \frac{\gamma\Omega}{\Gamma\omega}\right) \sinh^2\left(\frac{\Gamma L}{s}\right) - \left(1 - \frac{\Gamma\gamma}{\Omega\omega}\right) \sin^2\left(\frac{\Omega L}{s}\right),$$

$$\beta = 8 \sinh\left(\frac{\Gamma L}{s}\right) \sin\left(\frac{\Omega L}{s}\right)$$

$$k = (\Omega + i\Gamma) / s \quad \Omega = \sqrt{\frac{\sqrt{\omega^4 + \omega^2\gamma^2} + \omega^2}{2}}; \quad \Gamma = \sqrt{\frac{\sqrt{\omega^4 + \omega^2\gamma^2} - \omega^2}{2}}$$

Response is nonzero for  $U_a = U_b \rightarrow$  dc response induced by phase-asymmetry

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$$V = \frac{\beta \omega U_a^2 \sin \theta}{4U_g |\sin(kL)|^2 \sqrt{\omega^2 + \gamma^2}}$$

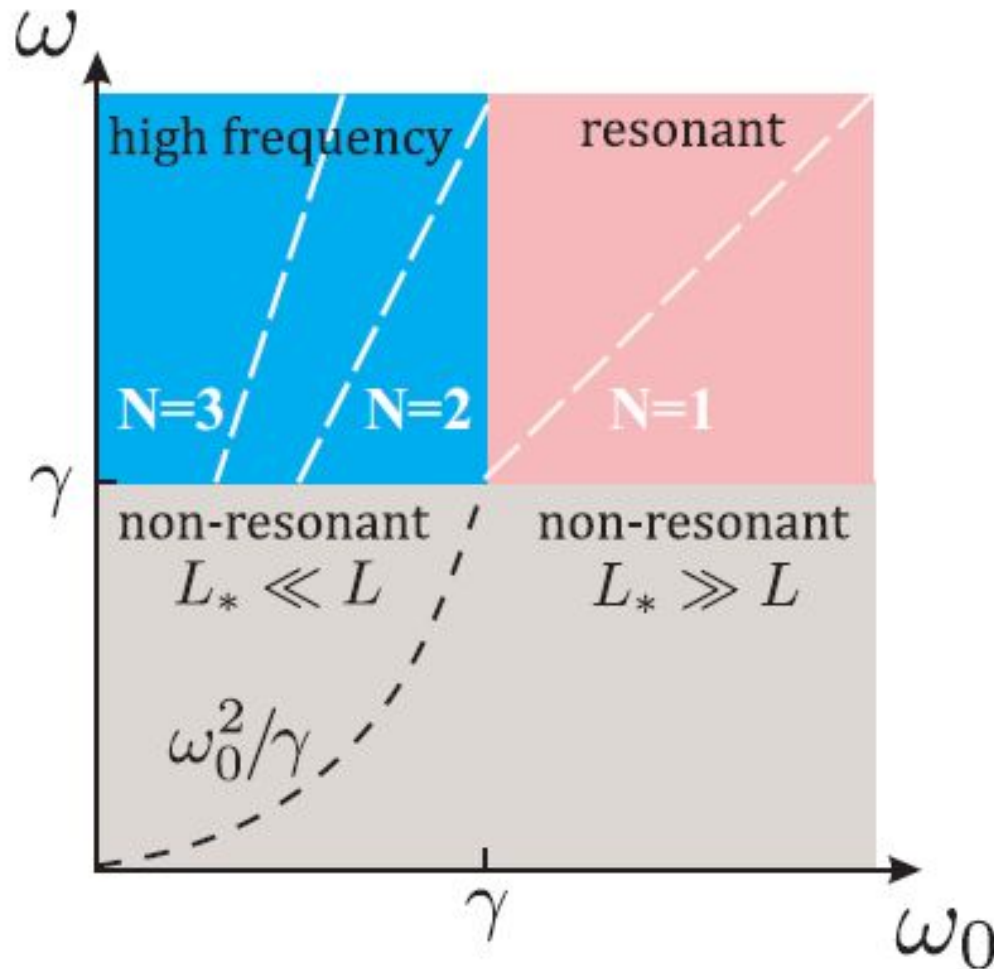
$$k = (\Omega + i\Gamma) / s$$

$$\Omega = \sqrt{\frac{\sqrt{\omega^4 + \omega^2 \gamma^2} + \omega^2}{2}}; \Gamma = \sqrt{\frac{\sqrt{\omega^4 + \omega^2 \gamma^2} - \omega^2}{2}}$$

$$\beta = 8 \sinh\left(\frac{\Gamma L}{s}\right) \sin\left(\frac{\Omega L}{s}\right)$$

# General diagram illustrating different regimes of TeraFET operation

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# Limiting cases: resonant case

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$\omega \gg \gamma, \omega_0 \gg \gamma$  where

$$\omega_0 = \frac{\pi S}{L}$$

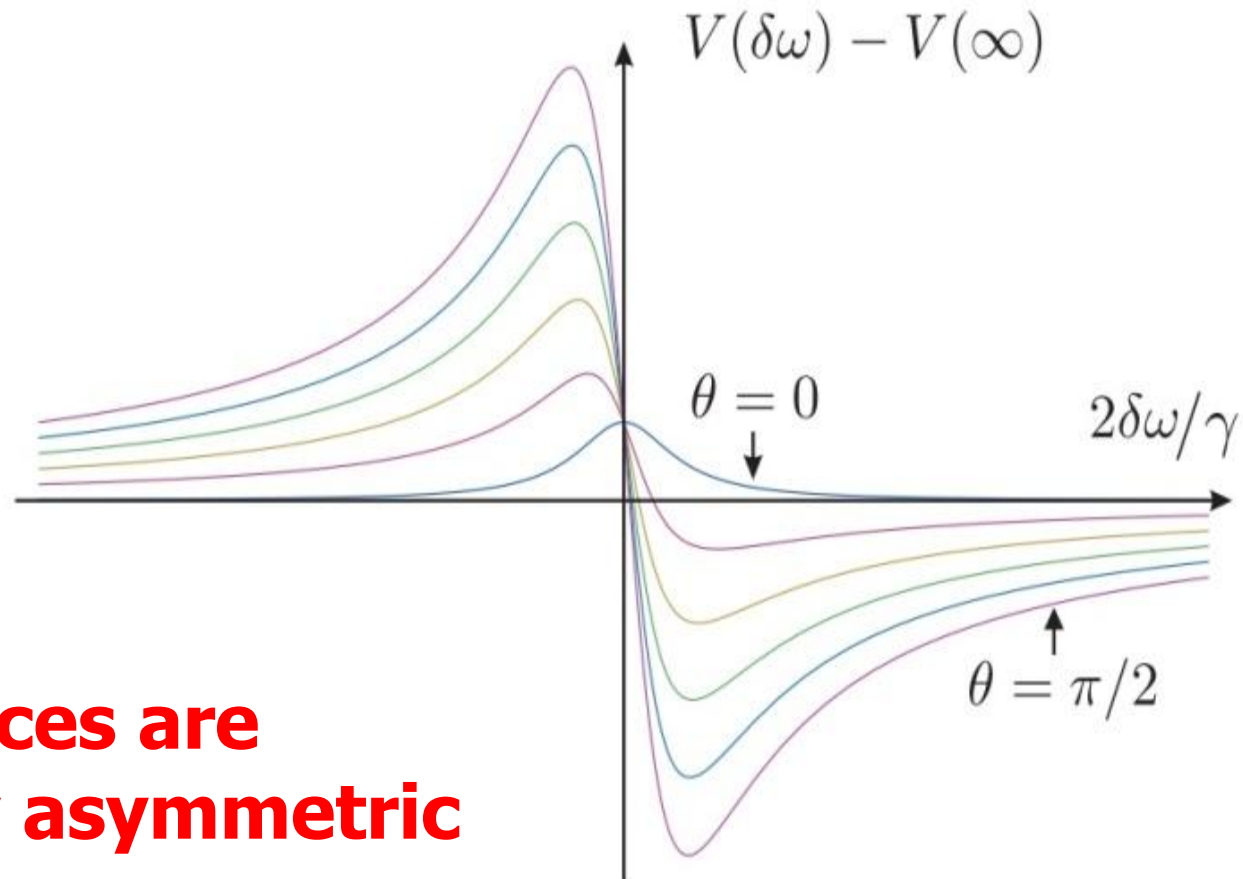
**fundamental plasma frequency**

**In vicinity of resonances**  $\omega \approx \omega_0: \delta\omega = \omega - \omega_0$

$$V(\delta\omega) = \frac{(U_a^2 - U_b^2)(3\gamma^2/4 - \delta\omega^2) + 4U_a U_b (-1)^N \delta\omega \gamma \sin\theta}{4U_g(\delta\omega^2 + \gamma^2/4)}$$

# Resonance dependence of dc response at a given frequency at different phase shifts $\theta$

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**resonances are strongly asymmetric**



# Limiting cases: high-frequency regime

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$$\omega_0 \ll \gamma \ll \omega, \quad k = \frac{\Omega + i\Gamma}{s} = \frac{\omega + i\gamma/2}{s}$$

$$V_{dc} = \frac{3(U_a^2 - U_b^2)}{4U_g} + \frac{4U_a U_b e^{-\gamma L/2s} \sin(\pi\omega/\omega_0) \sin\theta}{U_g}$$

**periodic oscillations  
with frequency**

# Limiting cases: high-frequency regime

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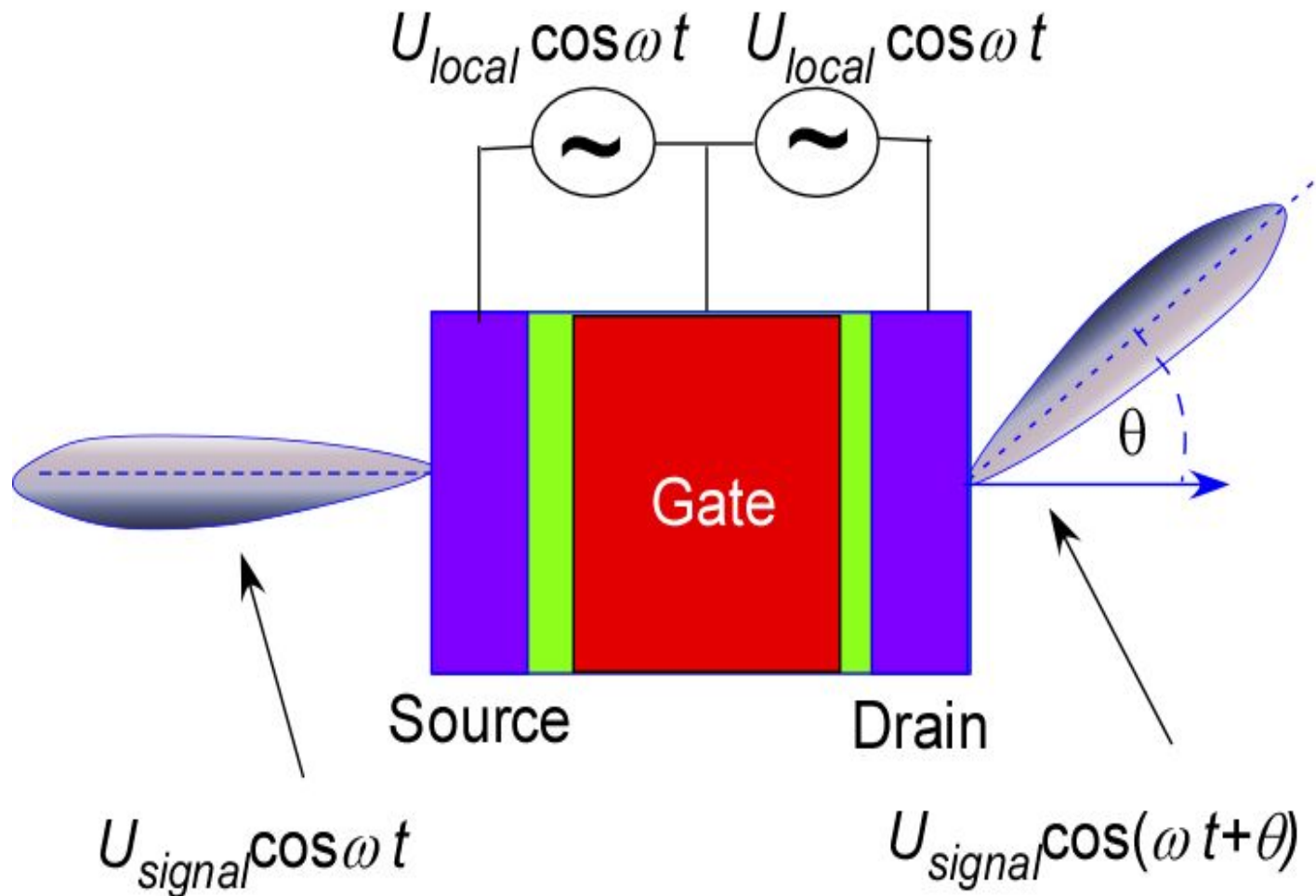
$$\omega_0 \ll \gamma \ll \omega, \quad k = \frac{\Omega + i\Gamma}{s} = \frac{\omega + i\gamma/2}{s}$$

$$V_{dc} = \frac{3(U_a^2 - U_b^2)}{4U_g} + \frac{4U_a U_b e^{-\gamma L/2s} \sin(\pi\omega/\omega_0) \sin\theta}{U_g}$$

**periodic oscillations  
with frequency**

# Homodyne detector operation scheme

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# Heterodyne operation scheme

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**Strong local oscillator**  $U_{local}$  + **weak phase-asymmetric signal**  $U_{signal}$

$$U_{local} \gg U_{signal}$$

$$U(0) = U_{local} \cos \omega t + U_{signal} \cos \omega t$$

$$U(L) = U_{local} \cos \omega t + U_{signal} \cos(\omega t + \theta)$$



$$U(0) = U_a \cos \omega t$$

$$U(L) = U_b \cos(\omega t + \tilde{\theta})$$

$$\theta = 0 \rightarrow \text{response} = 0$$

$$U_a = U_{local} + U_{signal}$$

$$U_b e^{i\tilde{\theta}} = U_{local} + U_{signal} e^{i\theta}$$

$$U_a^2 - U_b^2 = 2U_{local}U_{signal}(1 - \cos \theta)$$

→ **symmetric part**

$$U_a U_b \sin \tilde{\theta} \approx U_{local} U_{signal} \sin \theta$$

→ **asymmetric part**

# Response of Homodyne detector

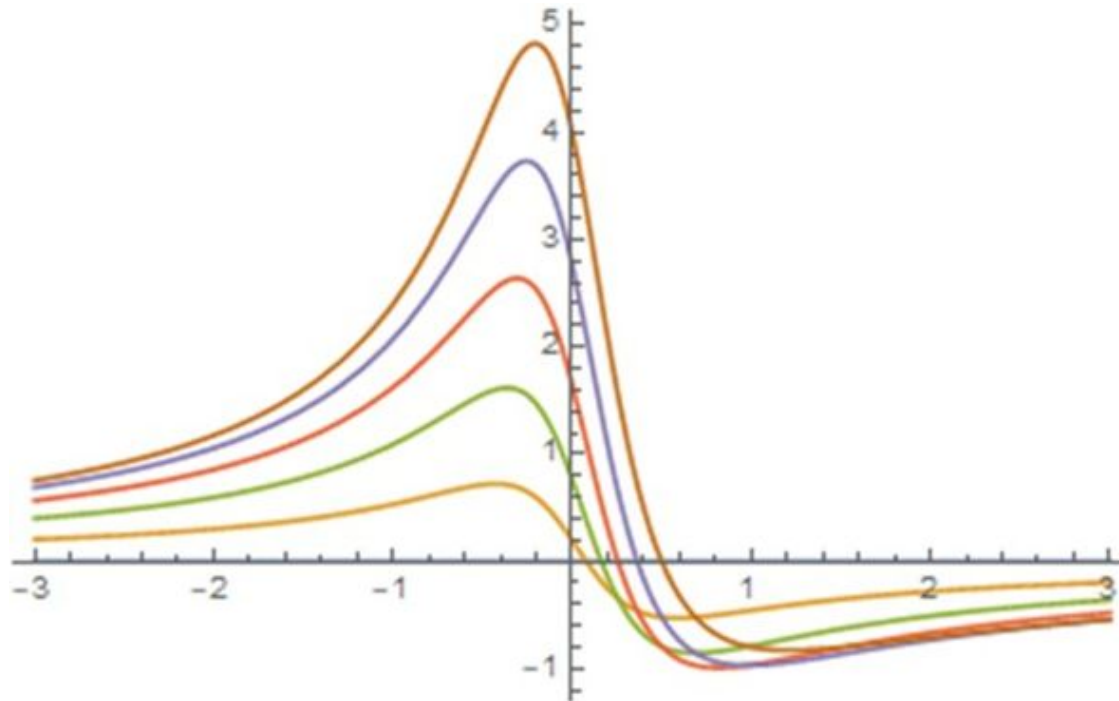
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$$V \approx \frac{U_{local} U_{signal}}{2U_g} \frac{(3\gamma^2 / 4 - \delta\omega^2)(1 - \cos\theta) + 2(-1)^N \gamma\delta\omega \sin\theta}{(\delta\omega^2 + \gamma^2 / 4)}.$$

# Response of Homodyne detector

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## Response



$\Delta\omega/$

$\gamma$

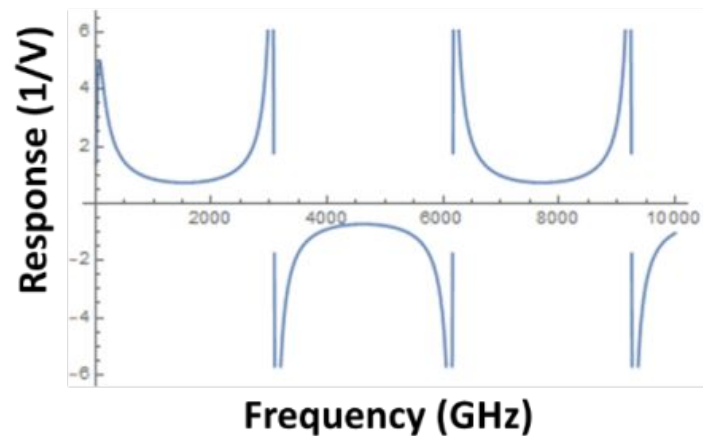
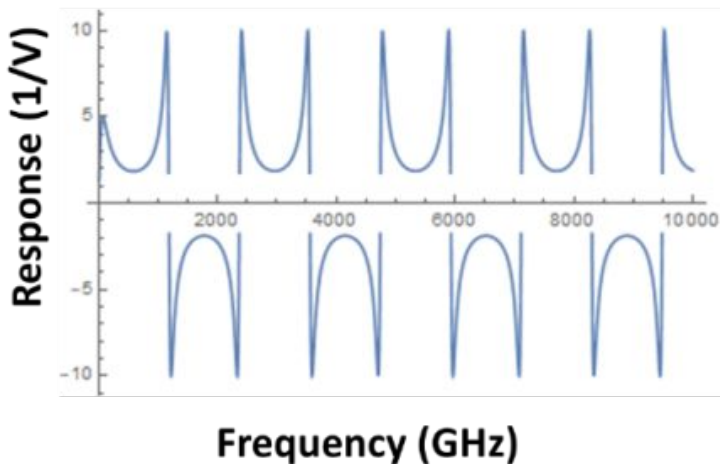
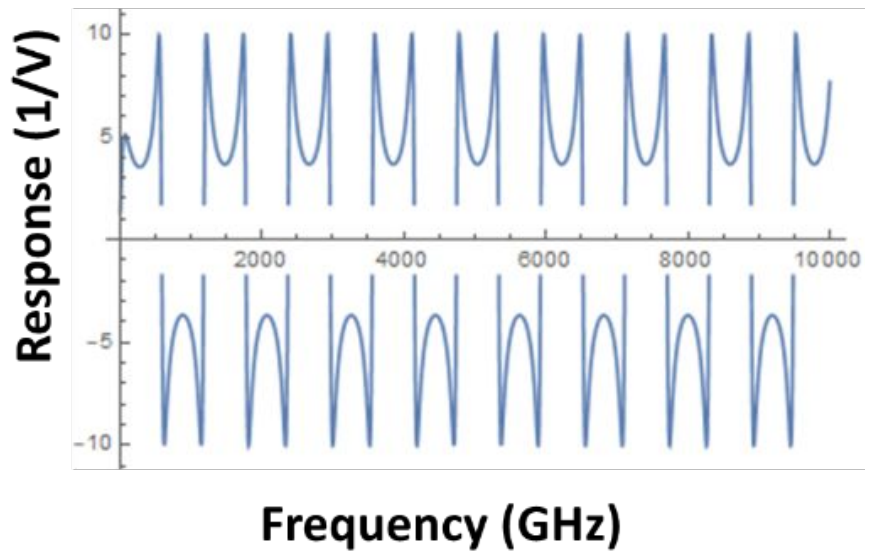
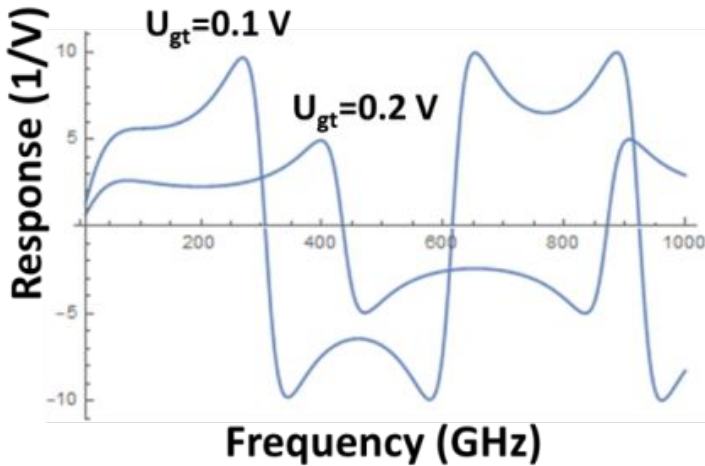
# MATERIALS PARAMETERS

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Material	Parameters	
	Effective mass	Mobility ( $\text{m}^2/\text{Vs}$ )
p-diamond	0.74	0.53
n-Si	0.19	0.10
n-GaN	0.24	0.15
n-InGaAs	0.041	0.8

# Diamond TeraFET response normalized to $U_a^2$ for $L=250$ nm (a), 130 nm (b), 65 nm (c) and 25nm (d)

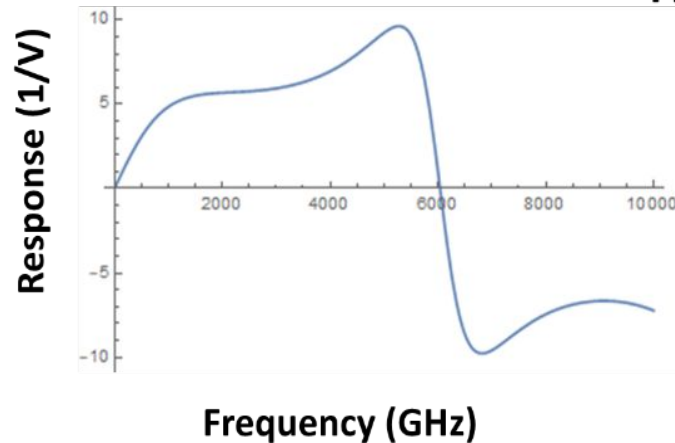
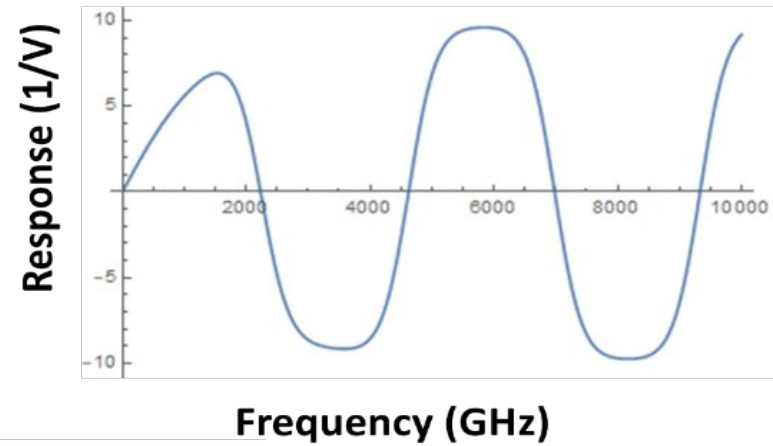
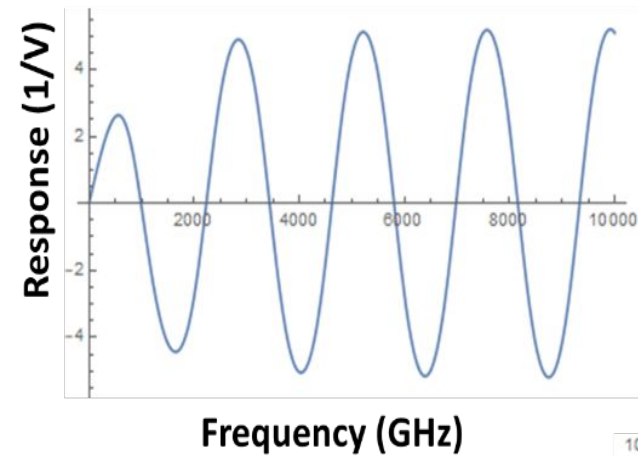
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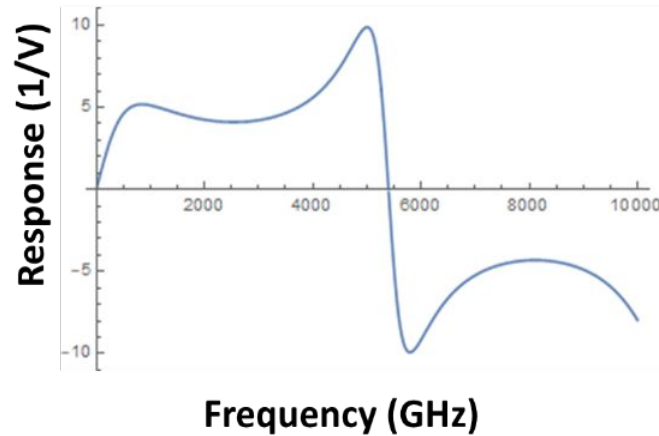
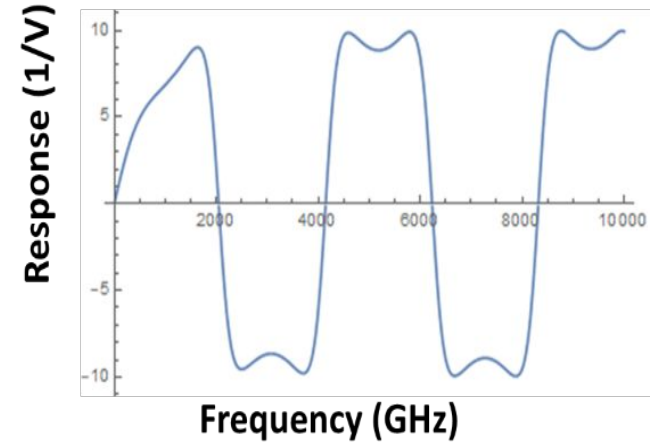
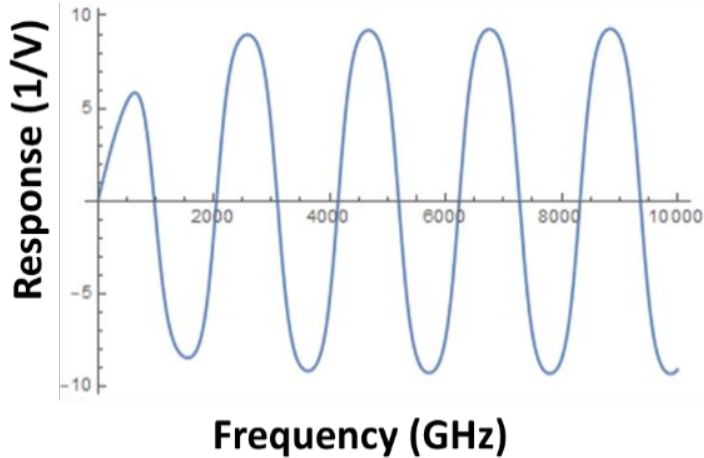
# Silicon TeraFET response normalized to $U_a^2$ for $L=130$ nm (a), 65 nm (b) and 25nm (c)

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# AlGaN/GaN TeraFET response normalized to $U_a^2$ for L=130 nm (a), 65 nm (b) and 25nm (c)

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# Conclusions

- ❑ **Phase-asymmetry-induced dc photoresponse in the FET subjected to THz radiation leads to sharp resonant peaks in vicinity of plasmonic resonances.**
- ❑ **The peaks have asymmetric shape as a function of frequency.**
- ❑ **Homodyne detection using phase asymmetry increases sensitivity by orders of magnitude**
- ❑ **These results can be used for creation compact, tunable spectrometers of THz radiation**

# Acknowledgment

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This work was made possible by Army Research Laboratory under ARL MSME Alliance (Project Manager Dr. Meredith Reed), by Army Research Office (Program Manager Dr. Joe Qiu) and by Office of Naval Research (Project Manager Dr. Paul Maki)



**Special thanks to NRL for  
2018 Distinguished Faculty  
Summer Fellowship**

