

An electro-thermal DMOS model validated on pulsed measurements



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Contents



- ***Introduction***
- ***Electro-thermal DMOS model***
- ***Thermal simulations on floorplan level***
- ***Conclusions***

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- **Introduction**
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Introduction



- ***Smart-power technologies:***

- Large power drivers (voltage $\sim 100\text{V}$, current $\sim 10\text{A}$)
- Sensitive analog circuits: interface to outside world
- Digital circuitry

- ***High local temperature due to:***

- High ambient temperature (example: automotive)
- High power dissipation (drivers)

- ***Importance of (electro-)thermal modelling:***

- Prediction of reliability issues: electro-migration, TDDDB, temp. enhanced BTI, triggering parasitic bipolar, bondwire reliability
- Device self-heating effects
- Impact of heating on (sensitive) neighbouring circuits

Contents



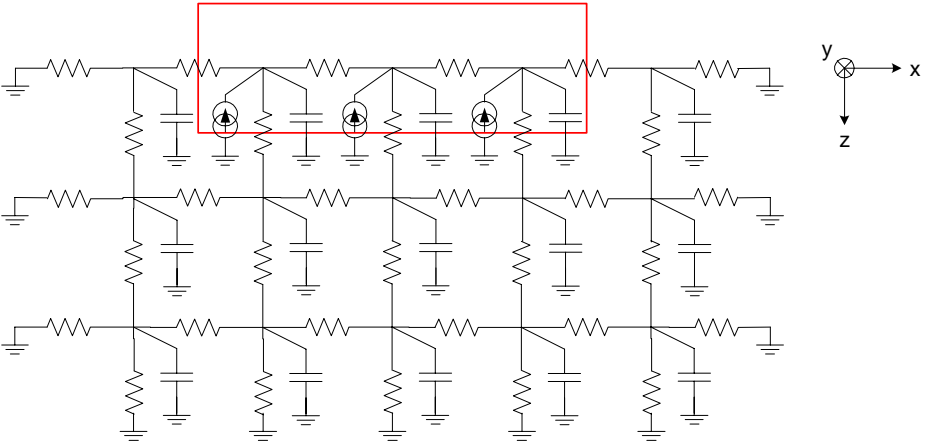
- *Introduction*
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Thermal RC-network

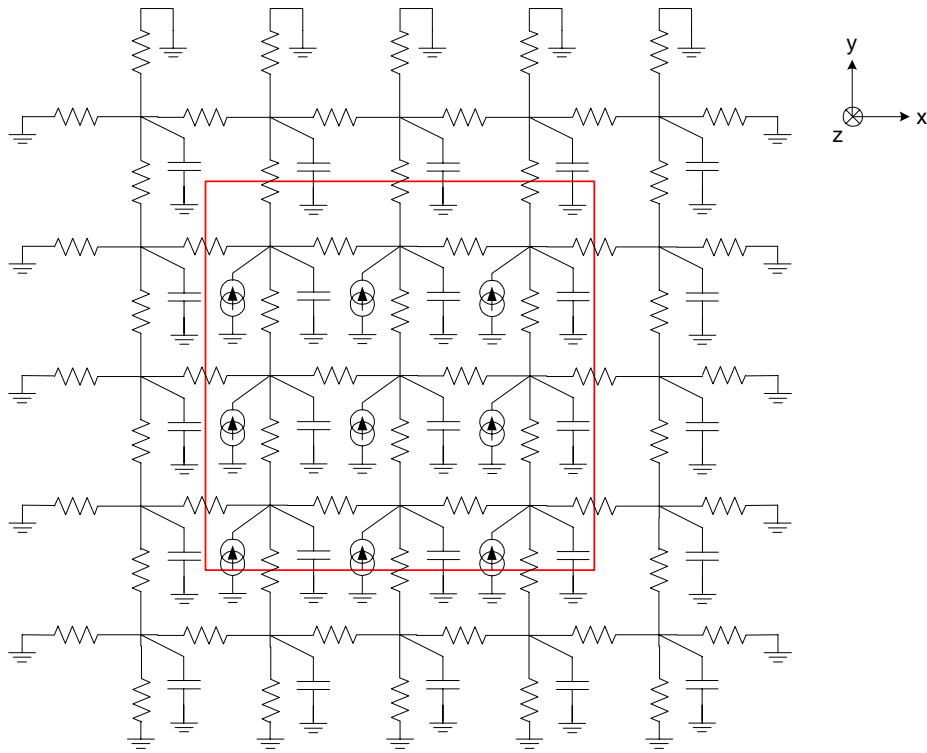


- Discretisation of space
- Modelling of thermal behaviour:
 - Resistors: heat conduction
 - Capacitors: heat storage
 - Current sources: heat generation

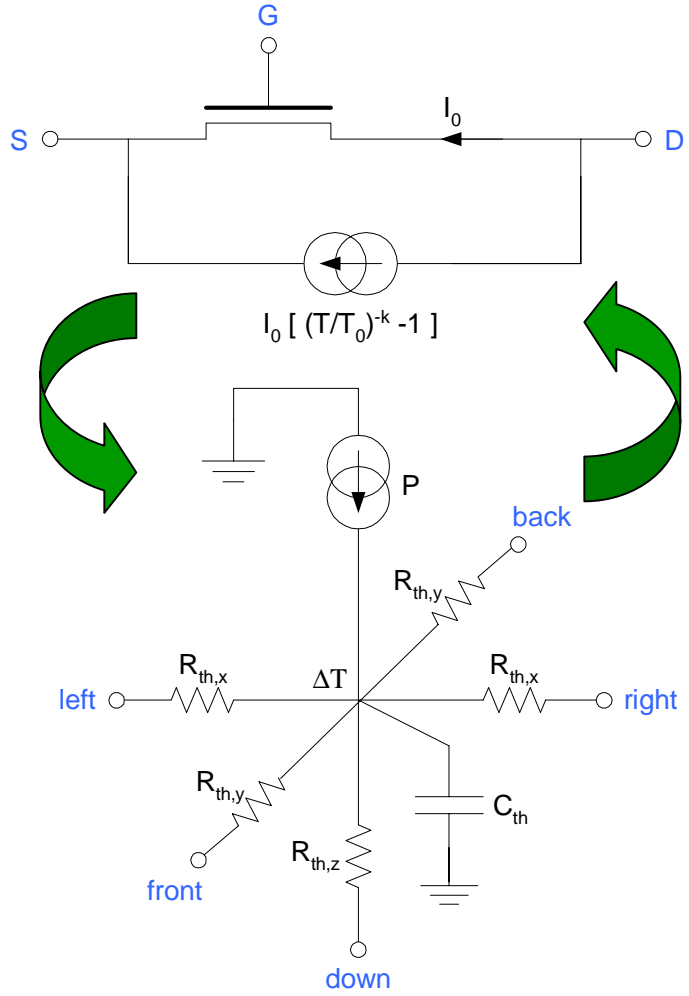
SIDE VIEW



TOP VIEW



Elementary electro-thermal cell



$$\frac{I}{I_0} = \left(\frac{T}{T_0} \right)^{-k}$$

coupling



electrical part



thermal part

Electro-thermal cell in Verilog-A



```
`include "discipline.h"
`include "constants.h"

module electrothermal_cell_3D (el_d, el_s, el_dd,
    th_left, th_right, th_front, th_back, th_up, th_down);

inout el_d, el_s, el_dd,
    th_left, th_right, th_front, th_back, th_down;

electrical el_d, el_s, el_dd;
thermal th_left, th_right, th_front, th_back, th_up, th_down,
    th_center;

parameter real rth_left = 1, rth_right = 1, rth_front = 1, rth_back
    = 1, rth_up = 1, rth_down = 1;
parameter real cth = 1;
parameter real k_exp = 1;

real temp_rise, I0, delta_I, I_tot, P0, P;
```

analog begin

```
temp_rise = Temp (th_center);

I0 = I (el_d, el_dd);
delta_I = I0 * (pow (1 + temp_rise / $temperature, - k_exp) - 1);
I_tot = I0 + delta_I;
```

```
P0 = I0 * V (el_d, el_s);
P = I_tot * V (el_d, el_s);
```

```
Pwr (th_center, th_left) <+ Temp (th_center, th_left) / rth_left;
Pwr (th_center, th_right) <+ Temp (th_center, th_right) / rth_right;
Pwr (th_center, th_front) <+ Temp (th_center, th_front) / rth_front;
Pwr (th_center, th_back) <+ Temp (th_center, th_back) / rth_back;
Pwr (th_center, th_up) <+ Temp (th_center, th_up) / rth_up;
Pwr (th_center, th_down) <+ Temp (th_center, th_down) /
    rth_down;
```

```
Pwr (th_center) <+ cth * ddt (temp_rise);
Pwr (th_center) <+ - P;
```

```
I (el_d, el_s) <+ delta_I;
```

end

endmodule

self-heating
effect

thermal
resistors

thermal
capacitance

Automatic generation of netlist



- **Full electro-thermal model: typical example:**
 - 15 x 15 lateral grid cells per layer
(5 x 5 for internal DMOS region)
 - 5 vertical layers
- **Automatic generation of netlist using Matlab program:**
 - Inputs:
 - ❖ material properties
 - ❖ number of grid cells
 - Output:
 - ❖ full generic netlist
 - ❖ all parameters in netlist scale with DMOS dimensions

Netlist electro-thermal DMOS model



```
simulator lang = spectre
```

```
inline subckt DMOS_self_heating (d g s)
```

```
parameters
```

```
+ w = 80
```

```
+ ns = 2
```

```
+ pitch = 8
```

```
+ W = w/ns
```

```
+ L = ns*pitch
```

```
+ rs = 40m
```

```
+ rd = 40m
```

```
+ k_exp=0.55
```

standard DMOS
model

```
t_1_1_1 (0 1_1_1 0 1_1_1 0 1_1_1) thermal_cell_3D rth_left=2000*W/L  
rth_right=333.333*W/L rth_front=2000*L/W rth_back=333.333*L/W  
rth_up=2.66667e+010/(W*L) rth_down=833333/(W*L) cth=6.524e-013*W*L
```

```
...
```

```
d_6_6_1 (dd_6_6_1 g s) fnd40b w=w/25 ns=ns rs=rs*25 rd=rd*25
```

```
t_6_6_1 (d s dd_6_6_1 5_6_1 6_6_1 6_5_1 6_6_1 0 6_6_1) electrothermal_cell_3D  
rth_left=333.333*W/L rth_right=333.333*W/L rth_front=333.333*L/W  
rth_back=333.333*L/W rth_up=2.66667e+010/(W*L) rth_down=833333/(W*L)  
cth=6.524e-013*W*L k_exp=k_exp
```

```
...
```

```
t_15_15_5 (14_15_5 0 15_14_5 0 15_15_4 0) thermal_cell_3D rth_left=20.8333*W/L  
rth_right=125*W/L rth_front=20.8333*L/W rth_back=125*L/W  
rth_up=1.33333e+007/(W*L) rth_down=8e+007/(W*L) cth=1.04384e-011*W*L
```

electro-thermal
cell model

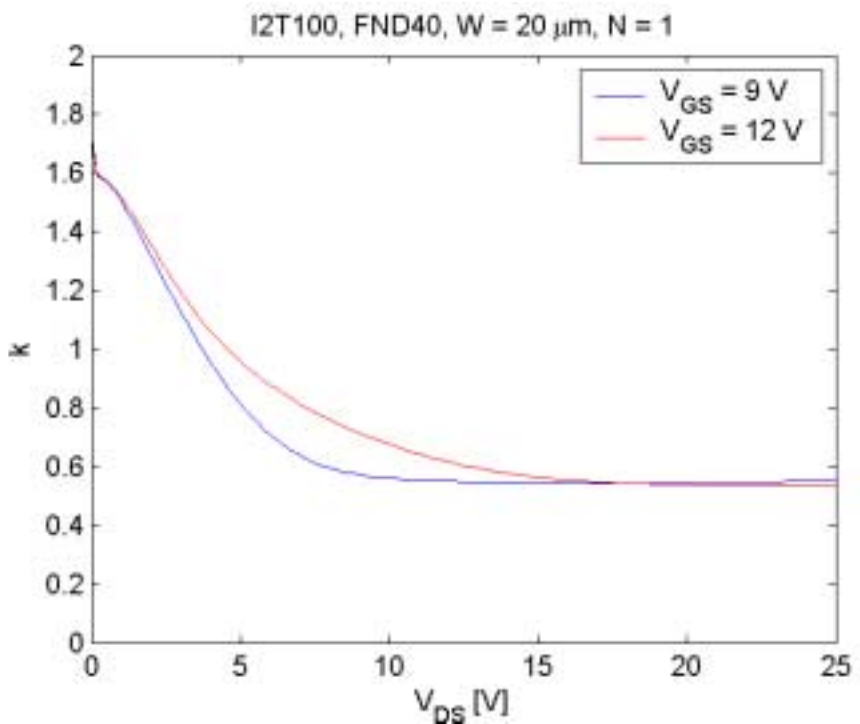
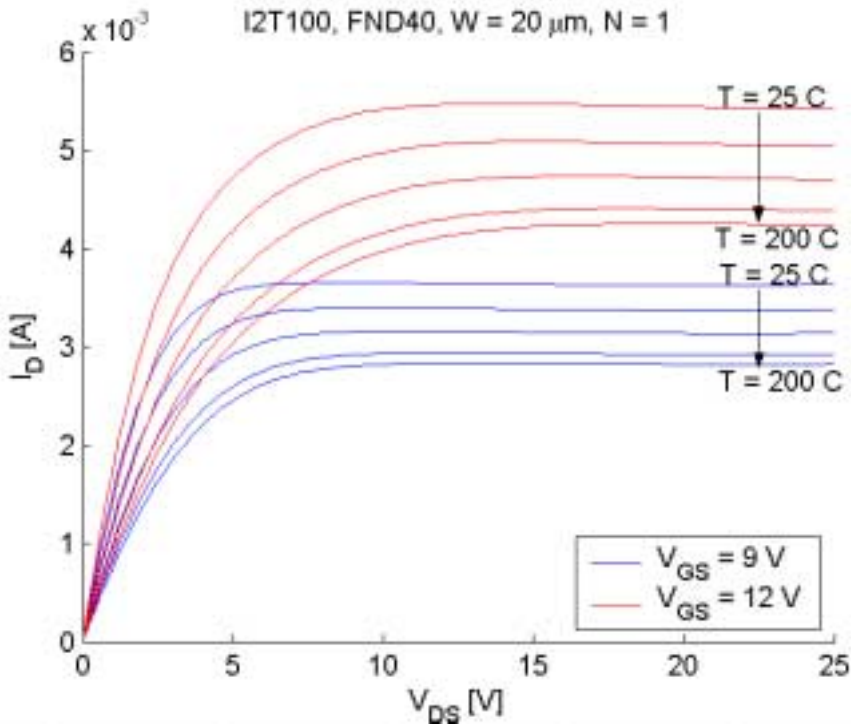
```
ends DMOS_SH
```

Extraction of exponent k



- Assumption: temperature dependence mainly attributed to mobility decrease
- Power law model
- Extraction of k on small devices

$$\frac{I}{I_0} = \left(\frac{T}{T_0} \right)^{-k}$$

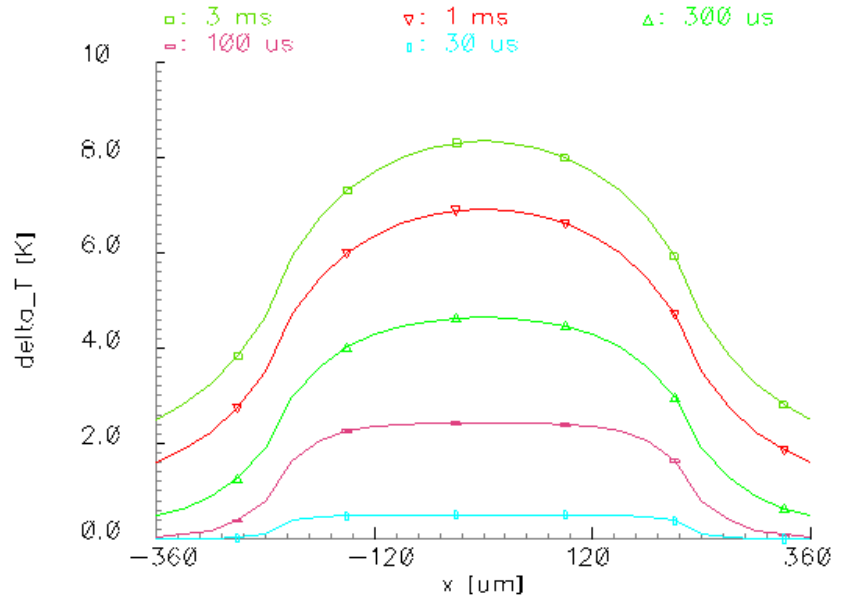


Results from Spectre simulation (1)

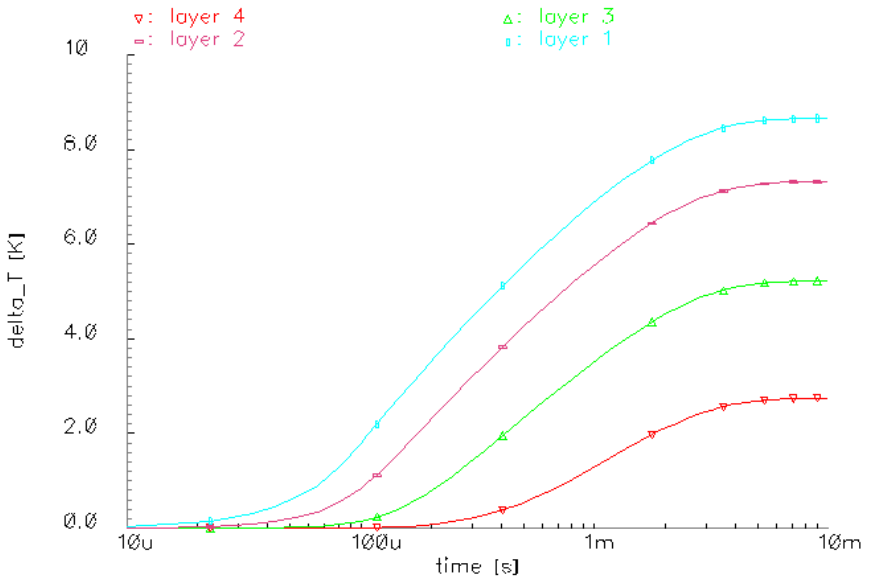


- Typical output from Spectre simulation for large driver ($W=450\mu\text{m}$, $L=450\mu\text{m}$, $P=1\text{W}$):

temperature through cross-section



temperature versus time

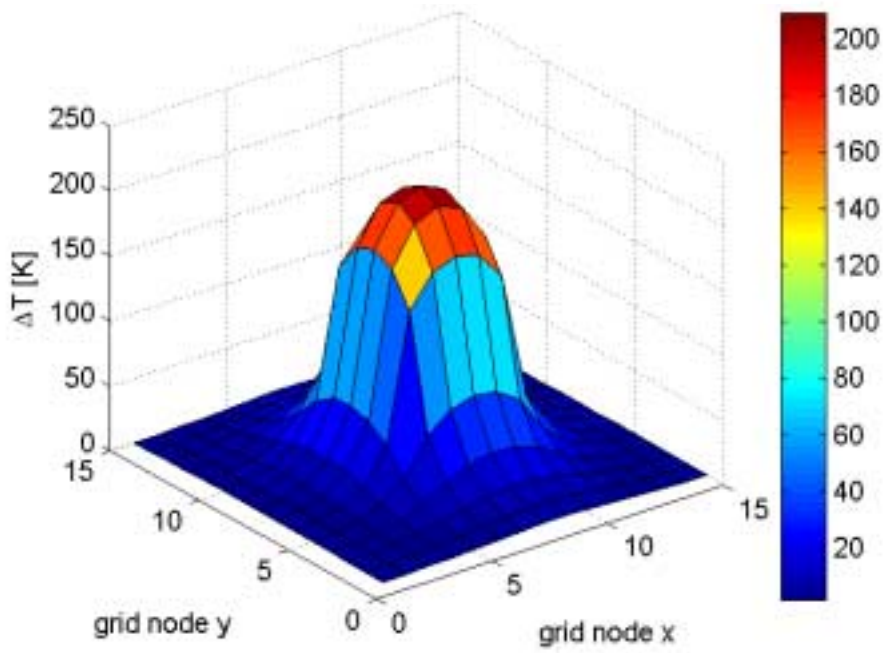


Results from Spectre simulation (2)

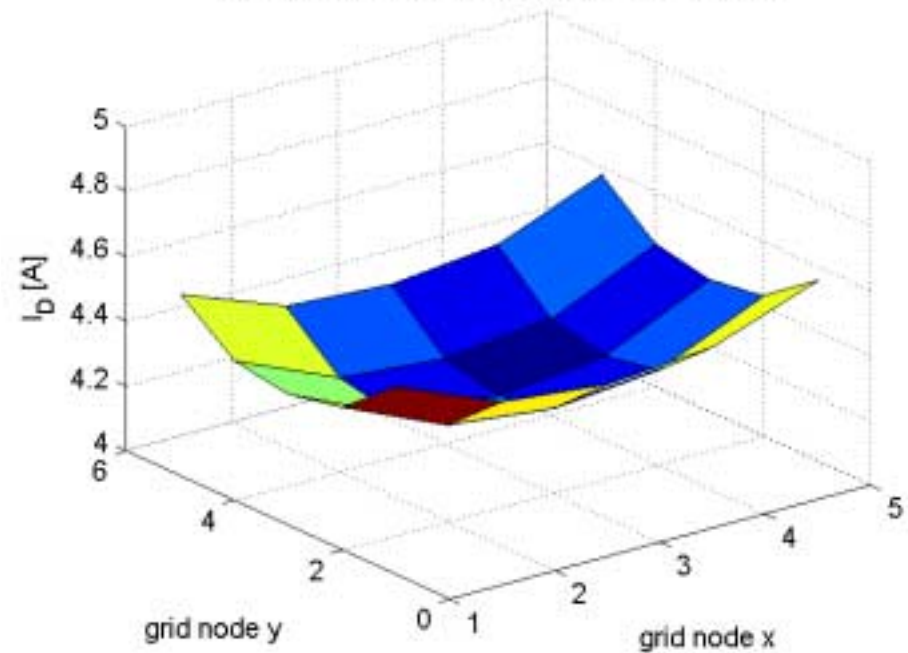


- Typical output from Spectre simulation for large driver ($W=450\mu\text{m}$, $L=450\mu\text{m}$, $V_{GS}=10\text{V}$, $V_{DS}=10\text{V}$, $t=500\mu\text{s}$):

temperature distribution



drain current distribution

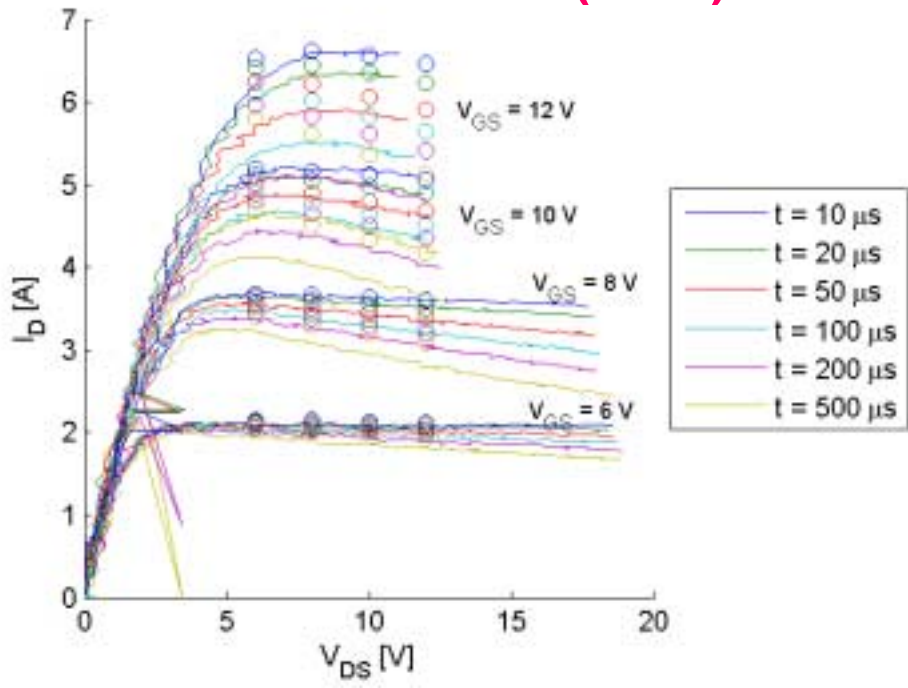


Comparison to measurements

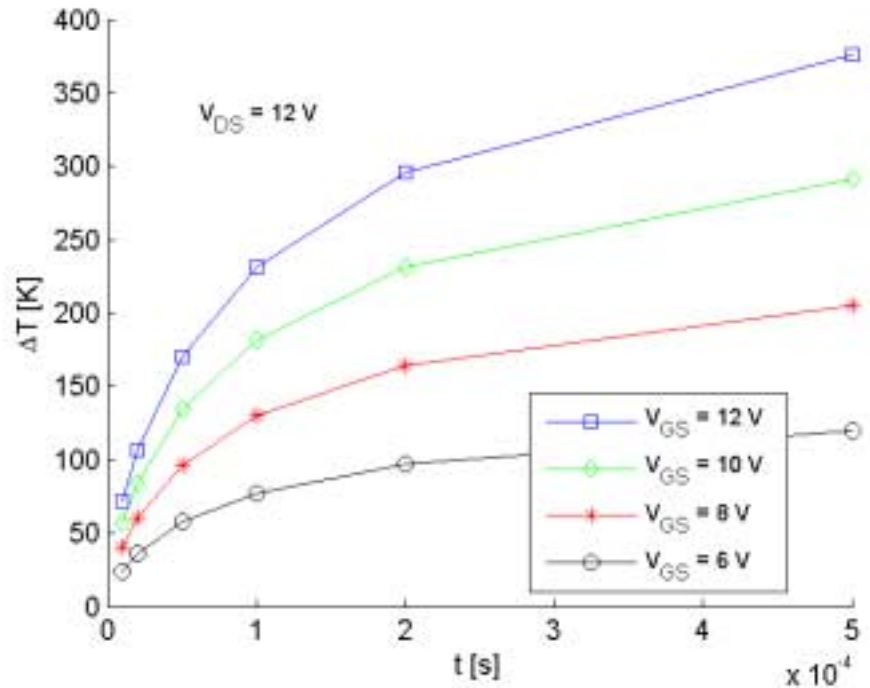


- Pulsed measurements on home-made energy capability set-up
- Used to characterise large devices

model (circles) versus measurements (lines)



model



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Thermal modelling approach (1)



Assumptions:

- rectangular, infinitely thin, homogeneous power source at top surface
- perfectly isolated top surface
- constant thermal conductivity (independent of temperature)

Exact analytical solution (based on Green's function):

$$\Delta T(x, y, z, t) = \frac{\sqrt{\alpha}}{4kWL\sqrt{\pi}} \int_{t'=0}^t \left[\operatorname{erf}\left(\frac{W/2+x}{\sqrt{4\alpha(t-t')}}\right) + \operatorname{erf}\left(\frac{W/2-x}{\sqrt{4\alpha(t-t')}}\right) \right] \\ \cdot \left[\operatorname{erf}\left(\frac{L/2+y}{\sqrt{4\alpha(t-t')}}\right) + \operatorname{erf}\left(\frac{L/2-y}{\sqrt{4\alpha(t-t')}}\right) \right] \\ \cdot \frac{1}{\sqrt{t-t'}} \cdot \exp\left(-\frac{z^2}{4\alpha(t-t')}\right) \cdot P(t') \cdot dt'$$

W, L: dimensions power source

k: thermal conductivity

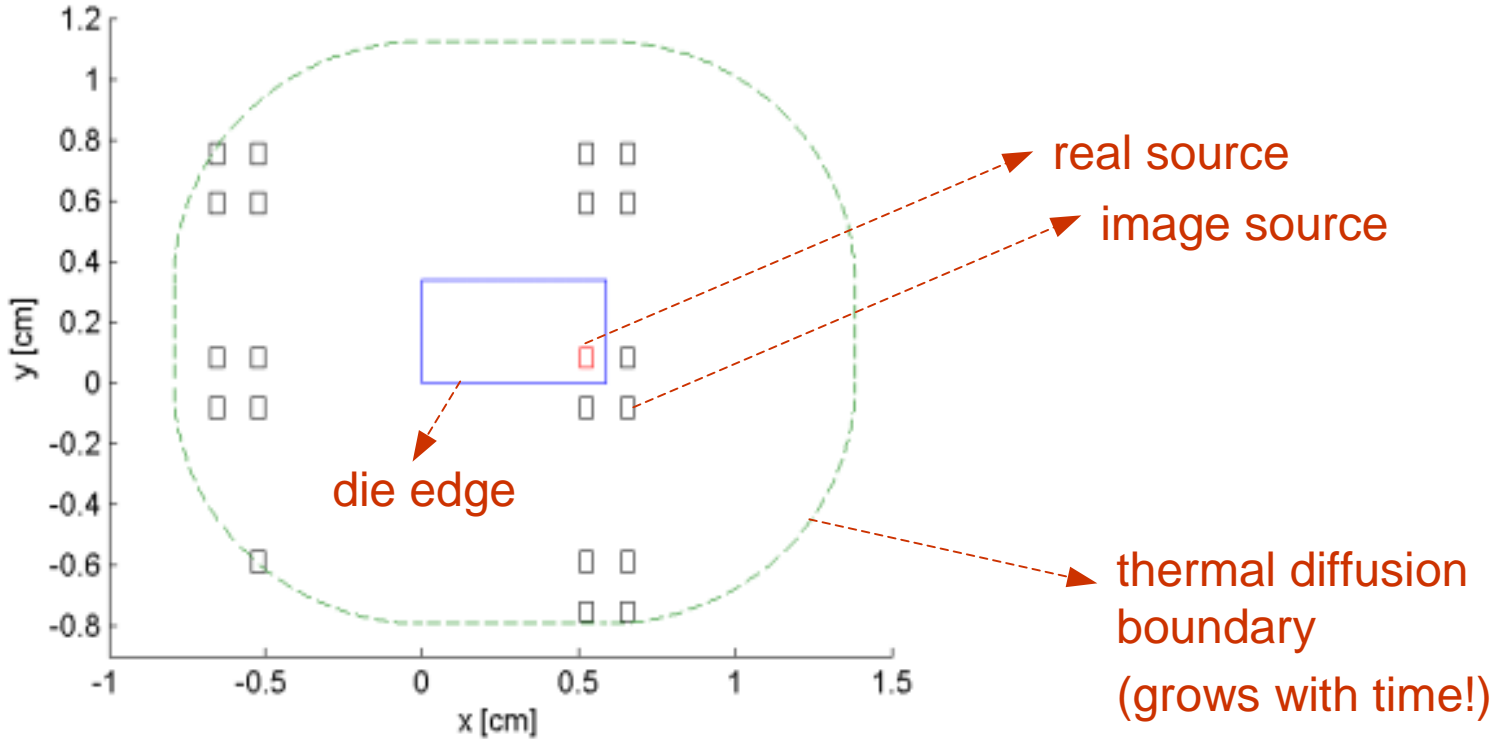
α : thermal diffusivity

P: power (any function of time)

Thermal modelling approach (2)



- Introduction of adiabatic die edges by superposition of solutions for array of **real** and **image** sources
- Only images within thermal diffusion boundary (limits simulation time)



User interface of thermal tool



power source positions

GUI temp_sim3_exp

File Help

Power sources

source name	x1 (um)	y1 (um)	x2 (um)	y2 (um)
source2	100	200	700	900

Die size

x1 (um)	y1 (um)	x2 (um)	y2 (um)
0	0	2200	2000

Sensors

sensor name	x (um)	y (um)
sensor1	400	550

Simulation setup

temperature distribution

simulation time vector (s): 100e-6

x-axis: 30, y-axis: 30

number of grid cells: 30x30

x1 (um)	y1 (um)	x2 (um)	y2 (um)
0	0	2200	2000

temperature evolution

simulation time vector (s):

Simulate and plot **SIMULATE !**

die size

sensor positions

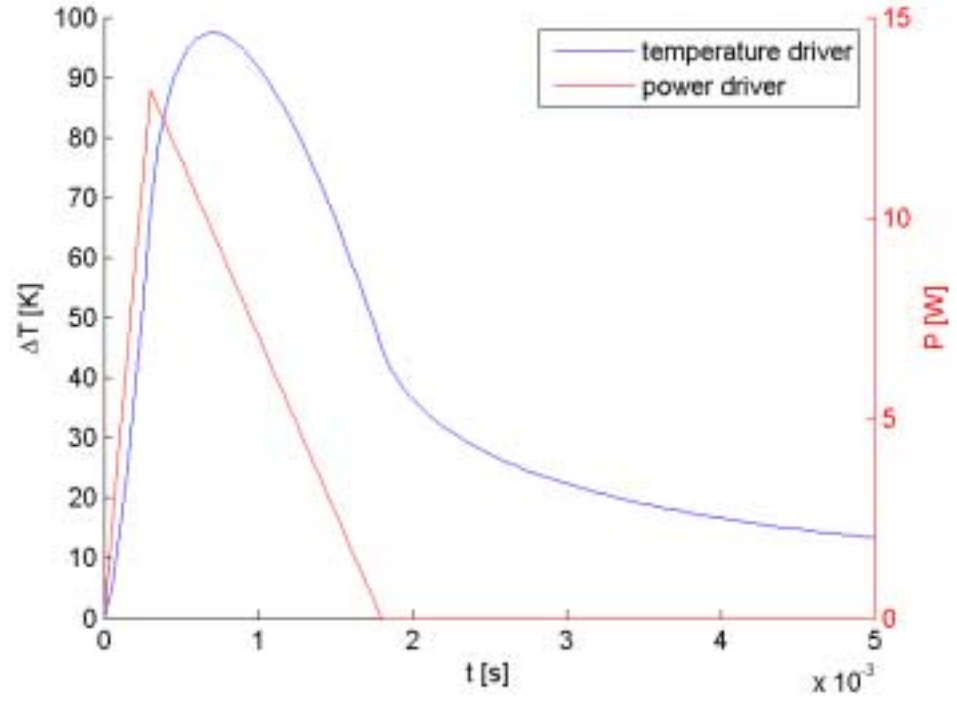
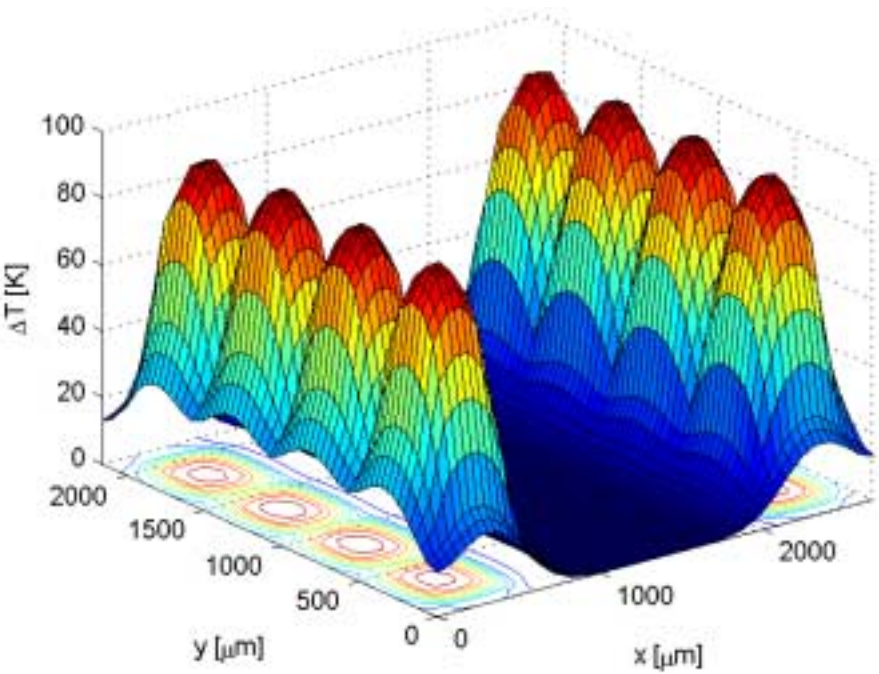
simulation grid and time

power waveforms

Typical application



- Simultaneous application of triangular power pulse to 8 large drivers:

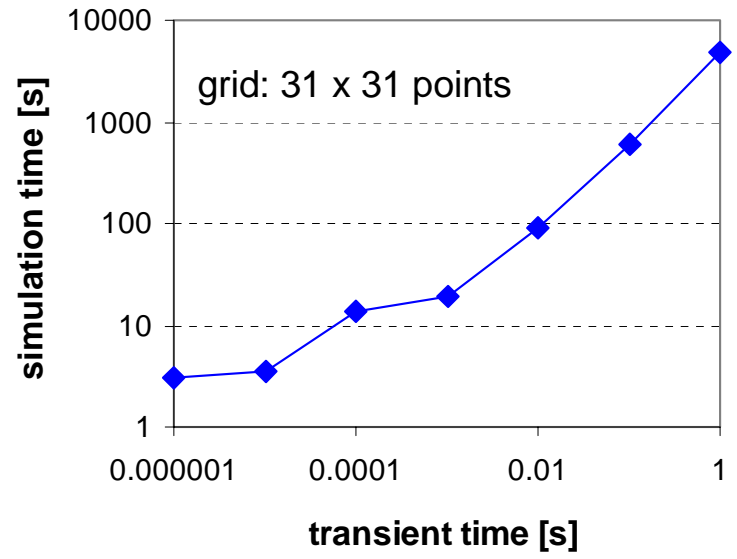


Speed / accuracy trade-off

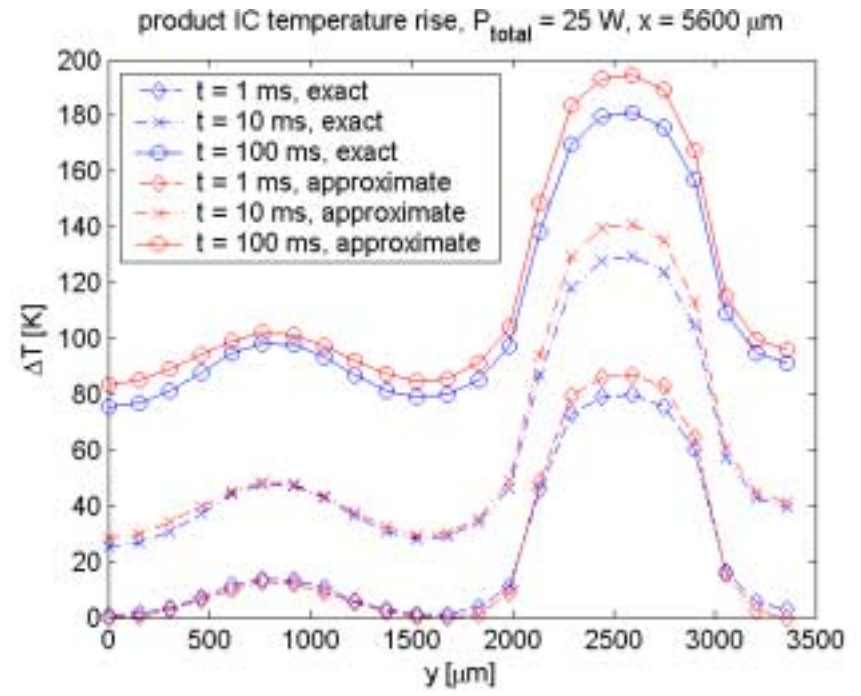


- Simulation time increase: due to increase of images
- Using approx. solution (only for power step function):
 - error: within 5%
 - speed increase: factor 30 !

simulation time exact solution



deviation approximate solution



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Conclusions



- ***Electro-thermal DMOS model:***

- Automatic generation of full netlist with RC-network
- Electro-thermal coupling using Verilog-A modules
- Model is scalable versus geometry
- Standard DMOS model is simply linked using a subcircuit
- Good correspondence with pulsed measurements

- ***Thermal simulations on floorplan level:***

- Fast and flexible Matlab tool with GUI
- Arbitrary number of arbitrary power waveforms
- Allows temperature evaluation on system level
- Results have been verified on products