

DE LA RECHERCHE À L'INDUSTRIE



HSP: A Surface-Potential-Based Compact Model of AlGaN/GaN HEMTs Power Transistors

Patrick Martin and Rereao Hahe

patrick.martin@cea.fr

**CEA, Leti, Silicon Components Division,
Simulation and Modeling Laboratory,
Minatec Campus, Grenoble, France.**

www.cea.fr

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- **Motivation**
- **Existing models for GaN power transistors, need for a more physical model**
- **GaN material specificity for power transistors**
- **HSP model flow**
- **AlGaIn/GaN energy band diagram and electrostatics**
- **Analytical E_F calculation, a tedious mathematical!**
- **Comparison of Numerical & Analytical E_F calculation**
- **Velocity saturation and mobility model**
- **Self-heating modeling**
- **Doping of AlGaIn by ion implantation**
- **Calculation of drain current**
- **Intrinsic charge model**
- **HSP model parameter list**
- **Results: parameter extraction, DC, self-heating**
- **Summary and conclusions**

- **Low cost, high performance devices used in energy conversion electronic circuits**
- **Applications: mainly switching applications, not analogue/RF amplification**
- **Low cost if substrate diameter greater than 4" - 100 mm (SiC)**
- **High performance: high switching speed**
- **GaN is a promising candidate for power applications (1200 V - 300 A, power ~ kW, high operating temperature about 250 °C)**
- **High breakdown field > 3 MV/cm**
- **High mobility in HEMT (High Electron Mobility Transistor)**
- **High electron saturation velocity: $1.2 \cdot 10^7$ cm/s**
- **Wide bandgap semiconductor**
- **AlGaN/GaN HEMTs**

Existing models for GaN power transistors

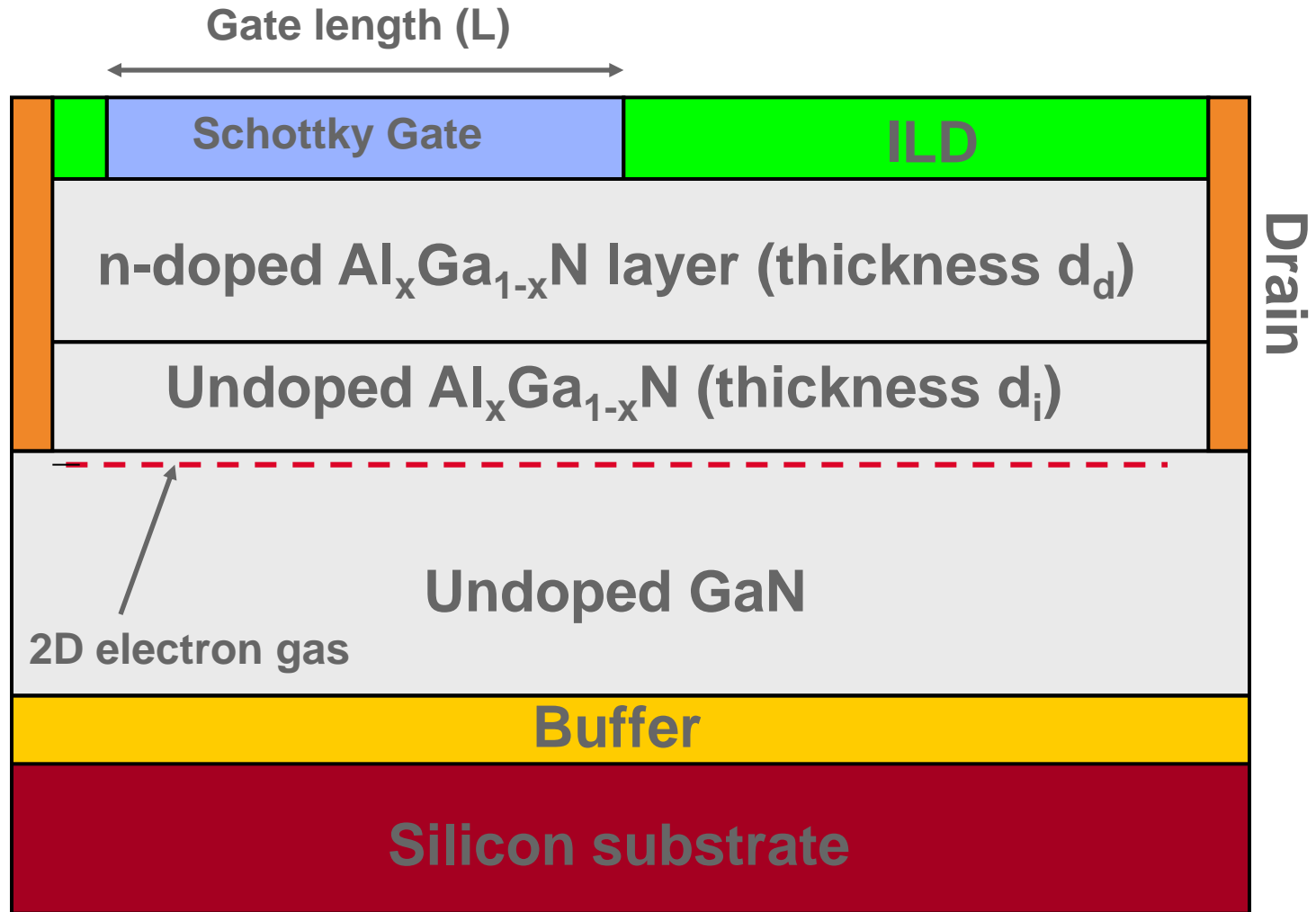
- **Macro-models using SPICE G source (or VCCS): one device, one set of parameters (e.g. EPC*)**
- **Empirical models such as cubic Curtice and Angelov (or Chalmers) models**
- **Threshold-voltage based, piece-wised model (weak, strong, moderate “inversion”)**
- **Surface-potential-based (since 2010-2011, John’10, Cheng’11, Khandelwal’12), iterative or analytical solving for Φ_s**
- **The last approach is relatively new and driven by analog/RF applications (need for accurate modeling of distortion in medium power amplifiers)**

*EPC: www.epc-co.com/

Need for a more physical model

- **A HEMT transistor is not a MESFET or a MOSFET (III-V compounds, inversion charge, mobility, ...)**
- **Many materials properties are Al-content and temperature dependent (E_g , σ , ...)**
- **Heterostructures growth technique has a strong impact on electrical properties**
- **HP devices will work at high temperature**
- **Self-heating effects will be very important**
- **Refractory compounds: donors are not fully ionized at RT, the ratio Nd^+/Nd is temperature-dependent**

AlGaN/GaN HEMT schematic structure



Lattice constants:

$a_{\text{Si}}=0.54 \text{ nm}$
 $a_{\text{GaN}}=0.32/0.51 \text{ nm}$
 (a/c axis)
 Important $\Delta a/a$

Thermal conductivity:

$K_{\text{Si}}=150 \text{ W/m.K}$
 $K_{\text{GaN}}=130$
 $K_{\text{SiC}}=320$

GaN material specificity for power transistors

- Large conduction band discontinuity ΔE_c between AlGaN and GaN: 2-Dimensional Electron Gas (2DEG)
- ΔE_c alone is not sufficient to explain very high charge sheet density of the 2DEG, in excess of 10^{13} cm^{-2} , even without intentional doping
- Additional effect: polarization-induced sheet carrier concentration leading to a strong confinement of 2DEG
 - 1 - Spontaneous polarization (SP) due to anion/cation in lattice, resulting electrical field=3 MV/cm
 - 2 - Piezoelectric polarization (PZ) proportional to strain:
 $\Delta a(x) = a(\text{Al}_x\text{Ga}_{1-x}\text{N}) - a(\text{GaN})$, electrical field=2 MV/cm
- Drawback: Normally-on transistors (depletion mode)
- Work in progress for normally-off HEMTs for safety reasons
- Only N-HEMTs

Contributions to the offset voltage

$$V_{off} = \Phi_B - \Delta E_c - \frac{q N_d d_d^2}{2 \epsilon_{Al_x Ga_{1-x} N}} - \frac{q \sigma}{\epsilon_{Al_x Ga_{1-x} N}} (d_d + d_i)$$

Total polarization σ (spontaneous + piezoelectric) is the main contribution to the offset voltage V_{off}

MOCVD: Ga face, MBE: N-face
Typical x_{Al} : 0.15-0.5
Donors: Silicon $N_d = 2 \cdot 10^{18} \text{ cm}^{-3}$

σ positive σ negative

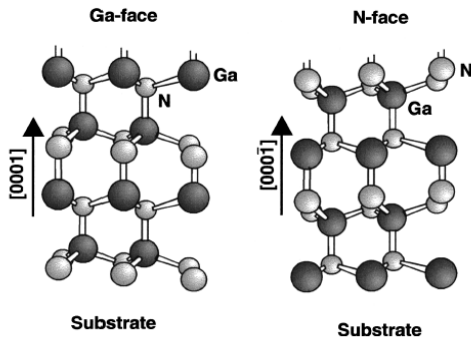
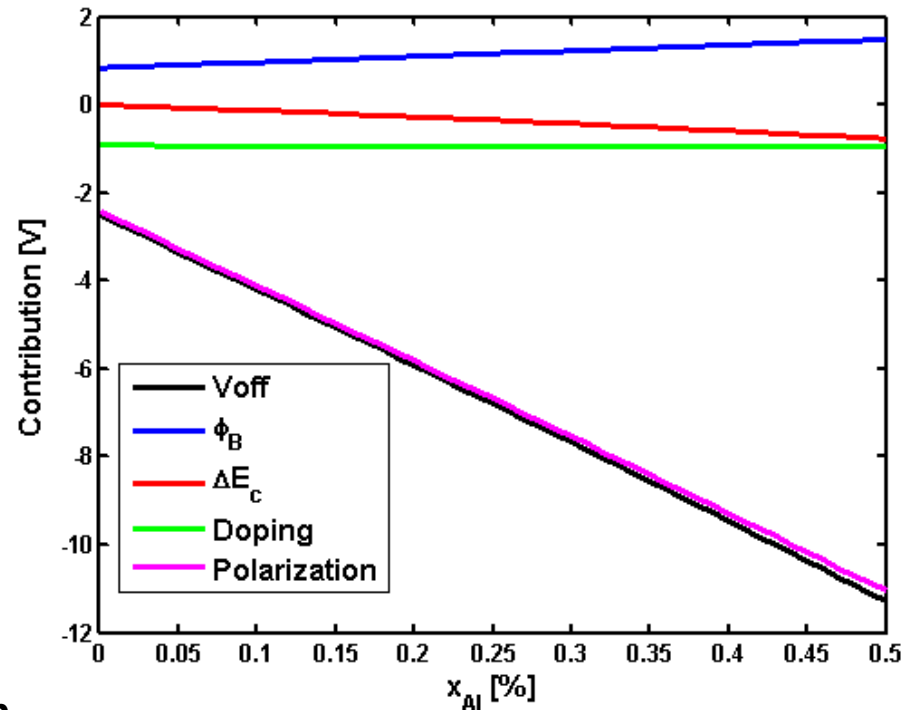
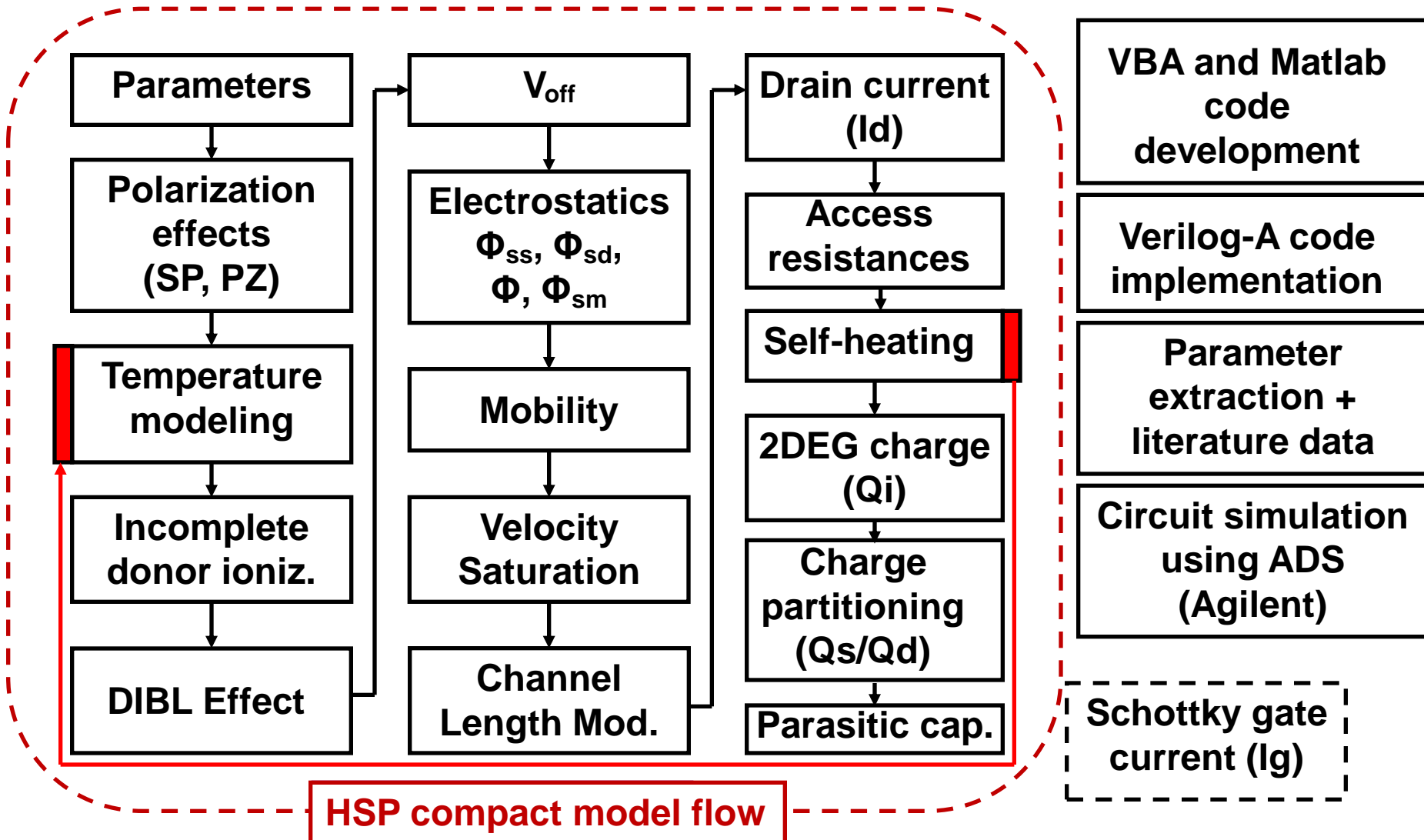


FIG. 4. Schematic drawing of the crystal structure of wurtzite Ga-face and N-face GaN.

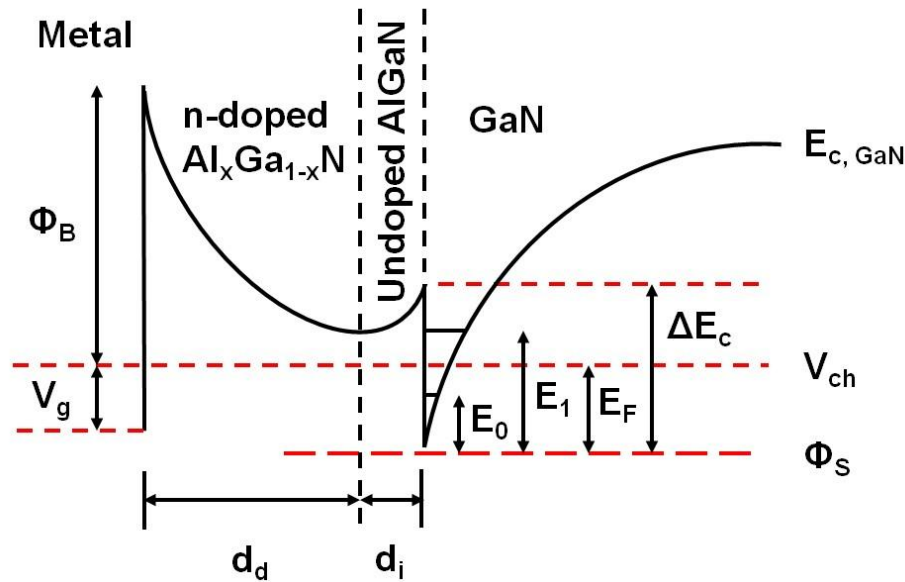


From Ambacher'99
Wurtzite= hexagonal form

A Surface-Potential-Based Compact Model of AlGaIn/GaN HEMTs Power Transistors: HSP model flow



AlGaN/GaN energy band diagram and electrostatics



Numerical resolution for E_F →

Assumptions:

- Triangular potential well
- Only the first quantum state, E_0 , is considered, E_1 is neglected

Self-consistent solving of Schrödinger's and Poisson's equations

2DEG sheet carrier concentration n_s :

$$\left\{ \begin{array}{l} n_s = \frac{\epsilon_{AlGaN}}{q d} (V_g - V_{off} - E_F) \\ n_s = D kT \text{Ln} \left[1 + \exp \left(\frac{E_F - E_0}{kT/q} \right) \right] \end{array} \right.$$

$$V_{off} = \Phi_B - \Delta E_c - \frac{q N_d d_d^2}{2 \epsilon_{AlGaN}} - \frac{q \sigma}{\epsilon_{AlGaN}} (d_d + d_i)$$

$$E_0 = C_0 n_s^{2/3}$$

$$D = 4 \pi m^* / h^2$$

Analytical E_F calculation

- Analytical determination of E_F is done in two steps:
- $E_F = \eta + \omega$
 - 1 - Approximate solution (η) for two asymptotic cases:
(a) for high n_s and (b) for low n_s
 - 2 - Small refinement (ω), important for medium n_s
- Refinement is done several times (5-10) to ensure good accuracy for medium n_s
- Surface-Potential (Φ_s) calculation: $\Phi_s = E_F + V_{\text{channel}}$
- At source: $\Phi_{ss} = E_F + V_s$, at drain: $\Phi_{sd} = E_F + V_d$

A tedious mathematical development around E_F analytical calculation!

Calcul du coefficient de raffinement w :

En écrivant notre solution $E_F = \eta + w$ et en modifiant l'équation (6) :

$$\ln\left(1 + \exp\left(\frac{(\eta + w) - u_1 (C_{ox} (v_{go} - \eta))^{2/3}}{v_g}\right)\right) = \frac{v_{go} - (\eta + w)}{a_1}$$

Cette équation que l'on fait passer en exponentielle est le point de départ du calcul de w :

$$1 + \exp\left(\frac{(\eta + w) - u_1 (C_{ox} (v_{go} - \eta))^{2/3}}{v_g}\right) = \exp\left(\frac{v_{go} - (\eta + w)}{a_1}\right)$$

Commençons par la partie droite de l'équation :

$$\exp\left(\frac{v_{go} - (\eta + w)}{a_1}\right) = \exp\left(\frac{v_{go} - \eta}{a_1}\right) \exp\left(\frac{-w}{a_1}\right)$$

en posant $\exp((v_{go}-\eta)/a_1) = e_2$ et en réécrivant le terme $\exp(-w/a_1)$ en utilisant un développement limité à l'ordre 2 :

$$\exp\left(\frac{v_{go} - (\eta + w)}{a_1}\right) = e_2 \left(1 - \frac{w}{a_1} + \frac{w^2}{2a_1^2}\right)$$

De la même manière pour le membre de gauche :

$$1 + \exp\left(\frac{(\eta + w) - u_1 (C_{ox} (v_{go} - \eta))^{2/3}}{v_g}\right) = 1 + \exp\left(\frac{(\eta + w)}{v_g}\right) \exp\left(\frac{-u_1 (C_{ox} (v_{go} - \eta))^{2/3} (1 - w/(v_{go} - \eta))^{2/3}}{v_g}\right)$$

En posant $\eta_1 = u_1 (C_{ox} (v_{go} - \eta))^{2/3}$:

$$= 1 + \exp\left(\frac{(\eta + w)}{v_g}\right) \exp\left(\frac{-\eta_1 (1 - w/(v_{go} - \eta))^{2/3}}{v_g}\right)$$

On fait alors un développement limité à l'ordre 2 du terme $(1 - w/(v_{go} - \eta))^{2/3}$ d'où

$$= 1 + \exp\left(\frac{(\eta + w)}{v_g}\right) \exp\left(\frac{-\eta_1}{v_g} \left(1 - \frac{2}{3} \frac{w}{(v_{go} - \eta)} - \frac{1}{9} \frac{w^2}{(v_{go} - \eta)^2}\right)\right)$$

En réorganisant les termes :

$$= 1 + \exp\left(\frac{(\eta - \eta_1)}{v_g}\right) \exp\left(\frac{w}{v_g} \left(1 + \frac{2}{3} \frac{\eta_1}{(v_{go} - \eta)}\right) + \frac{1}{9v_g} \frac{\eta_1 w^2}{(v_{go} - \eta)^2}\right)$$

On simplifie cette expression en posant $e_1 = \exp((\eta - \eta_1)/v_g)$ et $s_1 = - (2/3)(\eta_1/(v_{go} - \eta))$:

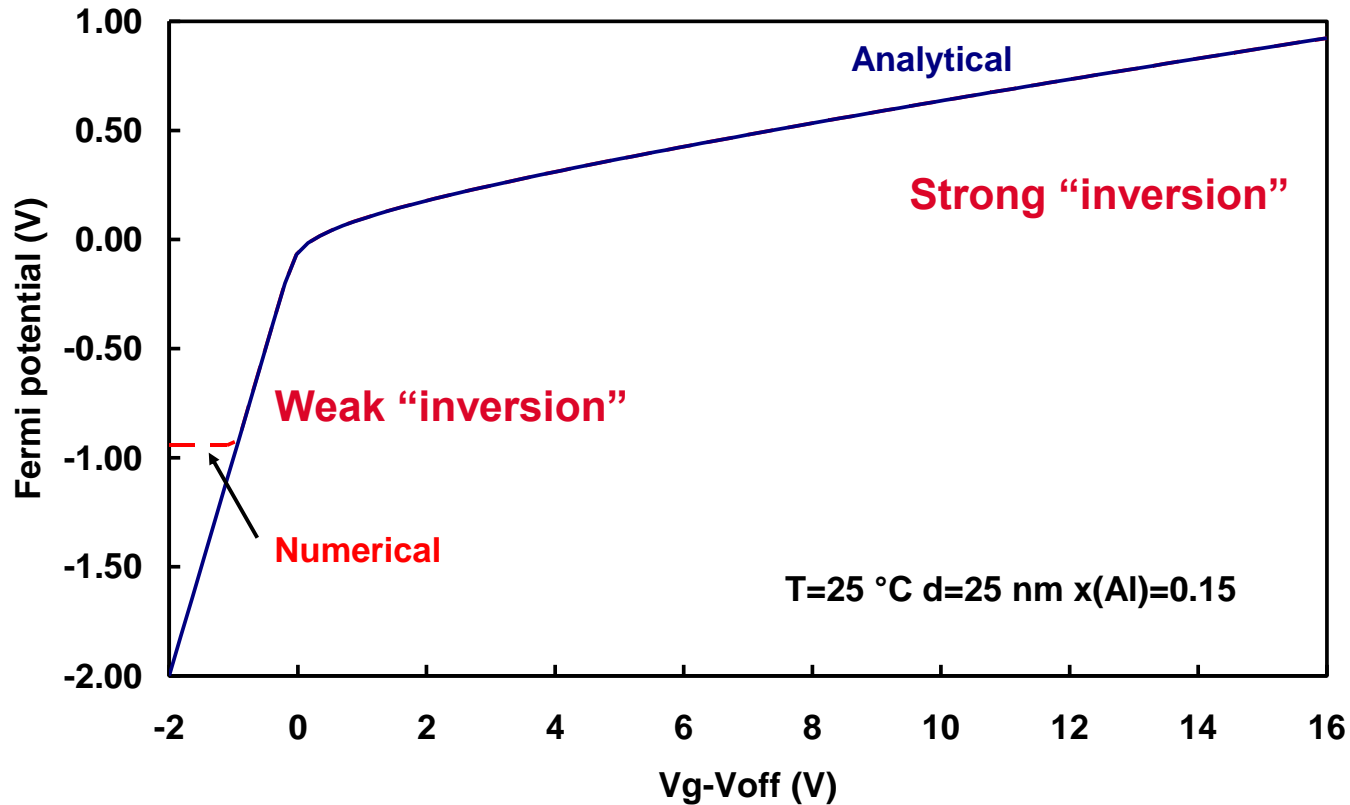
$$= 1 + e_1 \exp\left(\frac{w}{v_g} (1 - s_1)\right) \exp\left(\frac{1}{9v_g} \frac{\eta_1 w^2}{(v_{go} - \eta)^2}\right)$$

On recommence notre étape de développement limité des termes

$\exp\left(\frac{w}{v_g} (1 - s_1)\right)$ et $\exp\left(\frac{1}{9v_g} \frac{\eta_1 w^2}{(v_{go} - \eta)^2}\right)$ à l'ordre 2 et en négligeant les termes d'ordre

- We obtain different analytical expressions than Cheng'11: "A Surface-Based Compact Model for AlGaIn/GaN MODFETs"
- Our expressions are valid for very high Vds (1kV)

Comparison of Numerical & Analytical E_F calculation



- Numerical and analytical values of E_F are in great agreement
- Numerical calculation failed in very weak "inversion" as the triangular potential well assumption is no more valid

Velocity saturation and mobility model

- **Electron drift velocity and negative differential mobility in III-V semiconductors**
- **Much more simpler mobility model chosen in HSP:**

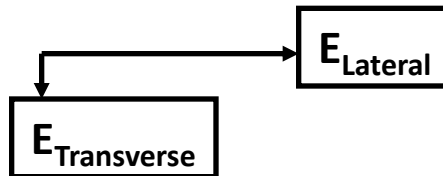
$$v_{drift}(E_L) = \frac{\mu_0 \cdot E_L + v_{sat} \left(\frac{E_L}{E_c}\right)^{n_1}}{1 + \left(\frac{E_L}{E_c}\right) + n_2 \left(\frac{E_L}{E_c}\right)^{n_3}}$$

$$v_{drift}(E_L) = v_{sat} \frac{\frac{|E_L|}{E_c}}{\left[1 + \left(\frac{|E_L|}{E_c}\right)^\alpha\right]^{\frac{1}{\alpha}}} = \mu_{LF}(E_T) \frac{|E_L|}{1 + \left(\frac{|E_L|}{E_c}\right)} \quad \text{for } \alpha = 1$$

$$P(T) = P_0 (a + bT + cT^2)$$

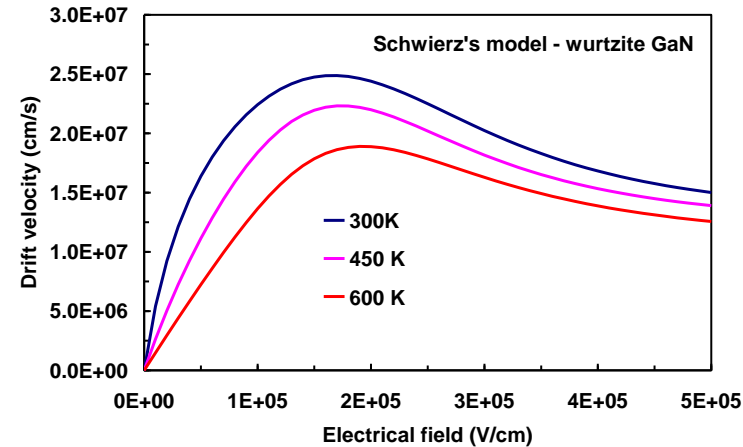
with $P = v_{sat}, E_c, n_1, n_2, n_3$

$$\mu_{LF}(E_T) = \frac{\mu_0}{1 + \alpha |E_T| + \beta E_T^2}$$



$$\epsilon_{GaN} \cdot E_T = \epsilon_{AlGaN} \cdot \frac{(Vg - V_{off} - \Phi_{sm})}{d}$$

From Gauss theorem at AlGaN/GaN interface



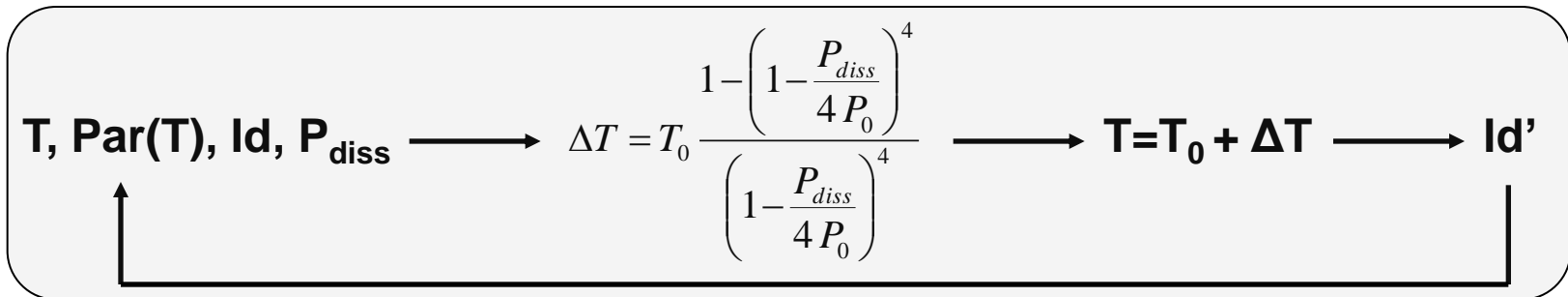
Velocity in bulk wurtzite (hexagonal) GaN

Self-Heating Effect (SHE) modeling

- Thermal conductivity
- 3 SHE models (SHEMOD)
 - 0 - No SHE
 - 1 - Constant Rth, no heat dissipation through substrate
 - 2 - With heat diffusion through substrate (thickness t_{sub}) and backside held at constant temperature T_0 (Canfield'90)
- Iterative calculation of drain current (SHEMOD=2)

$$\kappa(T) = \kappa(T_{ref}) \left(\frac{T}{T_{ref}} \right)^{KEX}$$

GaAs: KEX=-1.25
Si: KEX=-1.3
GaN: KEX=-1.4
SiC: KEX=-1.5



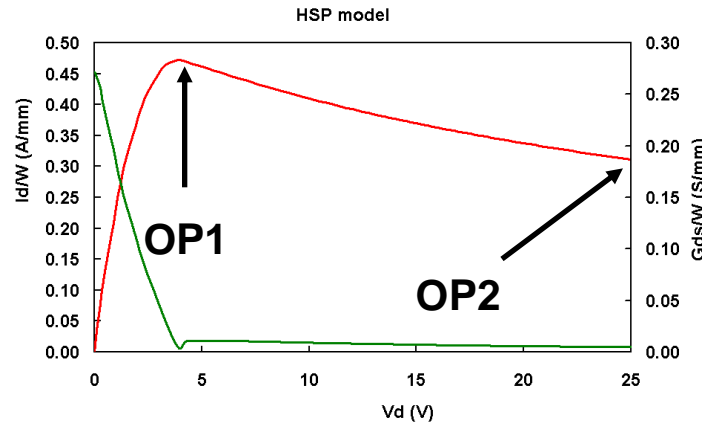
$$P_0 = \frac{\pi \kappa(T_0) W T_0}{Ln \left(\frac{8 t_{sub}}{\pi \alpha L} \right)}$$

$\alpha \leq 1$: effective transistor length where heat dissipation occurs (Royet'00)

If $\Delta Id / Id < 10^{-6}$ exit loop

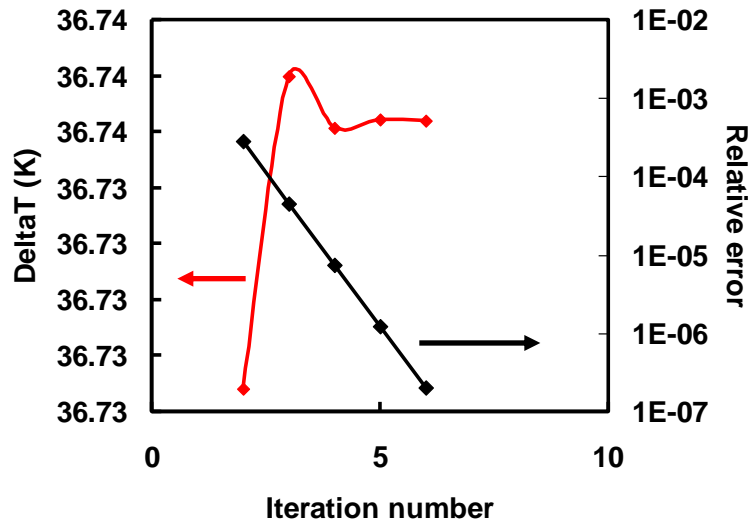
SHE: example of convergence

W=75 μm
L=1 μm
Vg=1 V
Temp=25 $^{\circ}\text{C}$

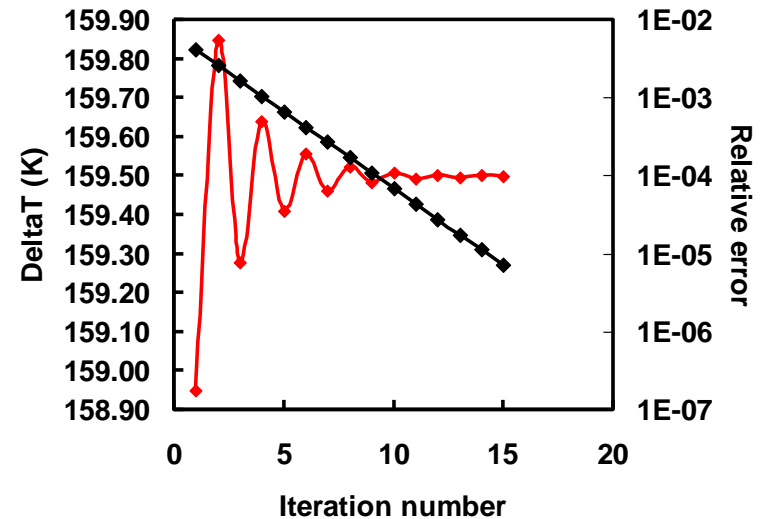


SHE_MOD=2
 $\alpha=1$
 $\kappa=150 \text{ W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$ (Si)
KEX=-1.3
Tsub=400 μm
T₀=25 $^{\circ}\text{C}$

OP1: 5 V, 35 mA, 0.17 W



OP2: 25 V, 23 mA, 0.58 W



Doping of AlGa_N by Silicon ion implantation

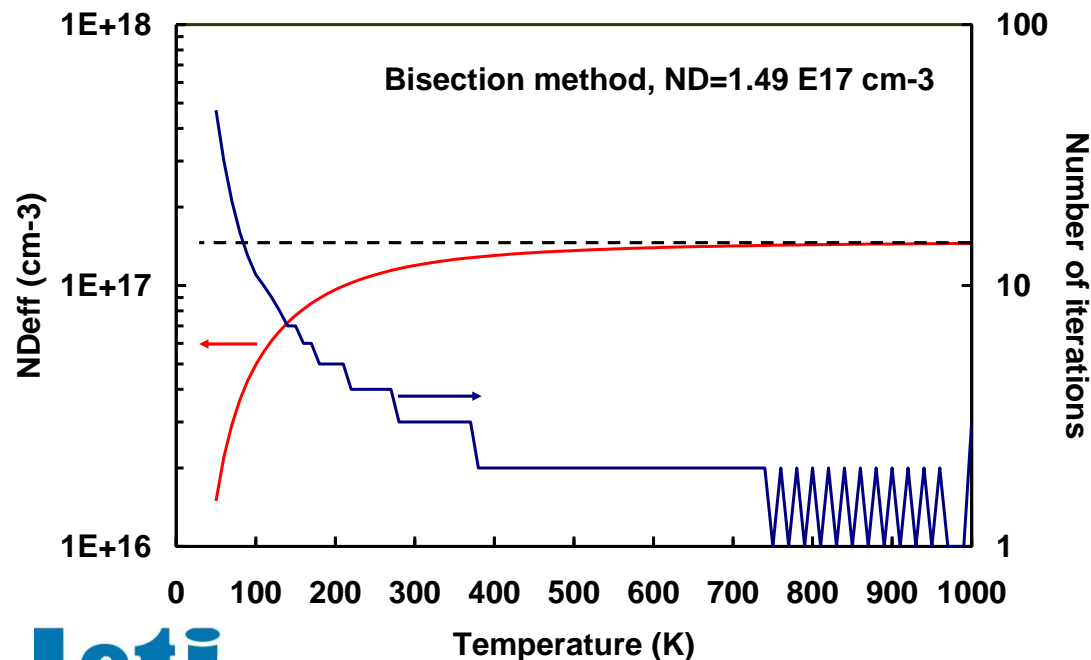
- Si substitutes for Ga in the lattice and acts as a donor
- Ionization of deep levels is incomplete at RT in refractory materials
- Two activation energies: $\Delta E_{D1}=12-17$ meV, $\Delta E_{D2}=32-77$ meV (Götz'96, GaN MOCVD films)
- Activation efficiency is function of implant temperature (Irokawa 2006): ~ 50 % at RT implantation
- Charge neutrality equation to be solved:

$$n(T) = \sum_{i=1}^n \frac{N_{Di}}{1 + \frac{g_i n(T)}{N_C(T)} \exp\left(\frac{\Delta E_{Di}}{kT}\right)} - N_A$$

- n: Effective donor concentration
- i: Index of donor
- g: Degeneracy (g=2)
- N_C : Density of states in CB
- N_D : Donor concentration
- ΔE_D : Donor activation energy
- N_A : Conc. of compensing acceptors

Silicon donors in GaN

- Charge neutrality equation solved by the bisection method
- $\Delta E_{D1}=15$ meV, $\Delta E_{D2}=37$ meV (Götz'96, GaN MOCVD films)
- $N_{D1}=1.1 \cdot 10^{17}$ cm⁻³, $N_{D2}=3.9 \cdot 10^{16}$ cm⁻³, $N_A=0$, $g_1=g_2=2$, $N_C=4.3 \cdot 10^{14} T^{1.5}$ cm⁻³ K^{-1.5}
- Three options in HSP (NDMOD):
 - 0: No partial ionization
 - 1: Partial ionization only during temperature modeling
 - 2: Partial ionization during temperature modeling and self-heating



$N_{Deff} / N_D = 80\%$ at RT
(activation efficiency=100%)

Ion implantation of Si in AlGaIn:
activation efficiency $\leq 50\%$
depending on implant
temperature (Irokawa'06)

Calculation of drain current in the HSP model

- Drain current calculation like in the silicon Surface-Potential (SP) model (G. Gildenblat'02) following Cheng's work (2011)
- Calculation of $\Phi_{ss} = E_F + V_s$ (source) and $\Phi_{sd} = E_F + V_d$ (drain)
- Drain current proportional to $\Phi = \Phi_{sd} - \Phi_{ss}$
- Use of the approach of symmetric linearization introduced in SP
- Use of $\Phi_{sm} = 0.5 * (\Phi_{ss} + \Phi_{sd})$, the SP midpoint for symmetry considerations (see Gummel symmetry tests)
- Our model includes:
 - 1 - Parameters temperature and x_{Al} dependency
 - 2 - DIBL effect (V_{off} shift with V_{ds} and L)
 - 3 - Velocity saturation and channel length modulation (CLM)
 - 4 - Self-heating via an iterative method
 - 5 - Incomplete donor ionization via bisection method
 - 6 - Access resistances (R_s, R_d)

$$I_{ds} = \beta \mu_{LF} \frac{(V_{gs} - V_{off} + V_t - \Phi_{sm}) \Phi}{r_L + \delta_0 \Phi / V_c}$$

HSP intrinsic charge model

- Importance of charge conservation in circuit simulation
- Calculation of Q_g
- Source and drain charges evaluated using the Ward-Dutton partitioning scheme
- If needed, capacitances will be calculated as derivatives of the terminal charges: $C_{ij} = -dQ_i/dV_j$ ($i \neq j$), $C_{ii} = dQ_i/dV_i$ ($i = j$)
- 9 transcapacitances, 6 are independent due to charge conservation: $Q_g + Q_s + Q_d = 0$

HSP model parameter list (1/2)

■ Setup parameters:

- DATAMOD AlGa_N material data
(Ambacher: 0, Yu: 1)
- VOFFMOD Set (0) or calculated (1) offset voltage
- VOFF Offset voltage

■ HEMT parameters:

- DD N-doped AlGa_N layer thickness
- DI Undoped AlGa_N layer thickness
- XAL Al content in Al_xGa_{1-x}N

■ AlGa_N doping:

- NDMOD Donor partial ionization (0-1-2)
- ND Donor concentration (NDMOD=0)
- G1 Degeneracy of the 1st donor level
- G2 Degeneracy of the 2nd donor level
- ED1 1st donor energy level
- ED2 2nd donor energy level
- ND1 1st donor concentration
- ND2 2nd donor concentration
- NA Acceptor compensating concentration
- AEFF Ion implantation activation efficiency

■ Geometrical parameters:

- L Gate length
- W Gate width
- DL Gate length offset
- DW Gate width offset

■ Mobility:

- MU0 Low field mobility
- P1 1st mobility attenuation parameter
- P2 2nd mobility attenuation parameter

■ Velocity Saturation & CLM:

- EC Critical electrical field
- UA VS parameter
- PVS VS parameter

■ DIBL effect:

- DIBL1 DIBL 1st parameter (V_{ds})
- DIBL2 DIBL 2nd parameter (Length)

HSP model parameter list (2/2)

▪ Self-heating effect:

- **SHEMOD** Self-heating mode (0-1-2-3)
- **RTH** Thermal resistance (SHEMOD=1)
- **REX** Thermal resistance temp. coeff.
- **CTH** Thermal capacitance
- **TSUB** Substrate thickness (SHEMOD=2-3)
- **ALPHA** Fraction of channel length for power dissipation (SHEMOD=3)
- **KAPPA** Substrate thermal conductivity
- **KEX** Thermal conductivity temp. coeff.

▪ Access resistances:

- **RS** Source resistance
- **RD** Drain resistance

▪ Temperature effects:

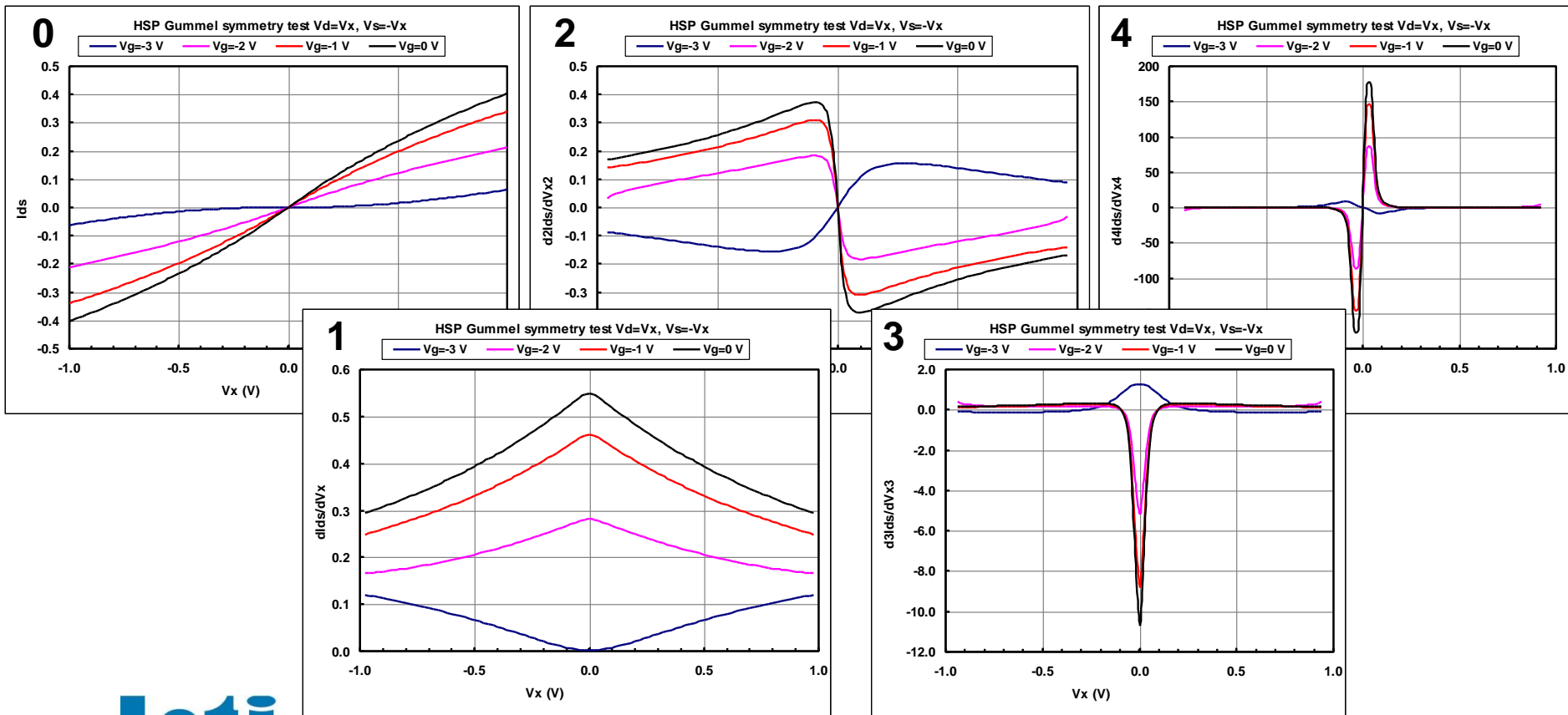
- **TNOM** Nominal temperature
- **TCV** VOFF temp. coeff.
- **MUEX** Mobility temp. coeff.
- **ECEX** EC temp. coeff.
- **TR1** Resistance 1st temp. coeff.
- **TR2** Resistance 2nd temp. coeff.

▪ Overlap & fringing capacitance:

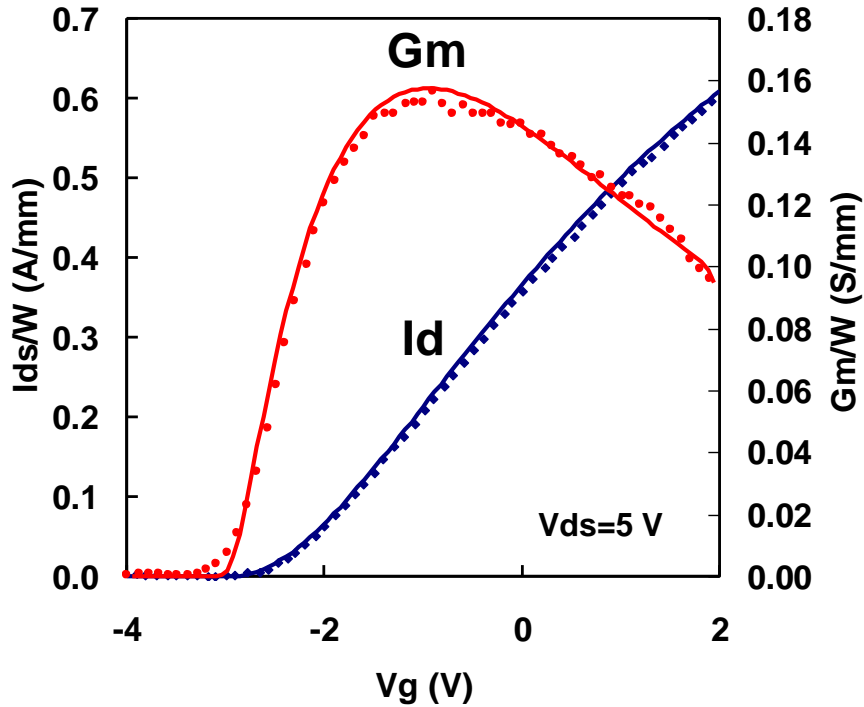
- **COV** Overlap cap.

Results: Gummel symmetry tests (GST)

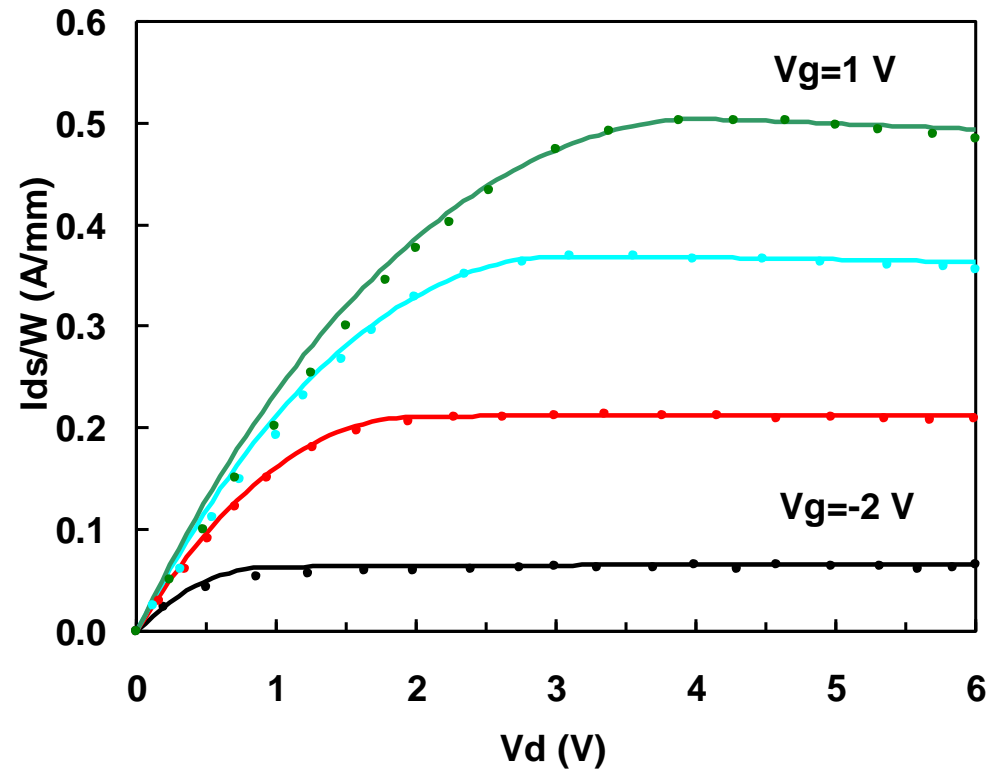
The drain current I_d is an odd function of V_x . Consequently, all odd order derivatives of $I_d(V_x)$ with respect to V_x should be continuous at $V_x=0$, and all even order derivatives should be equal to zero at $V_x=0$



Results: Parameter extraction

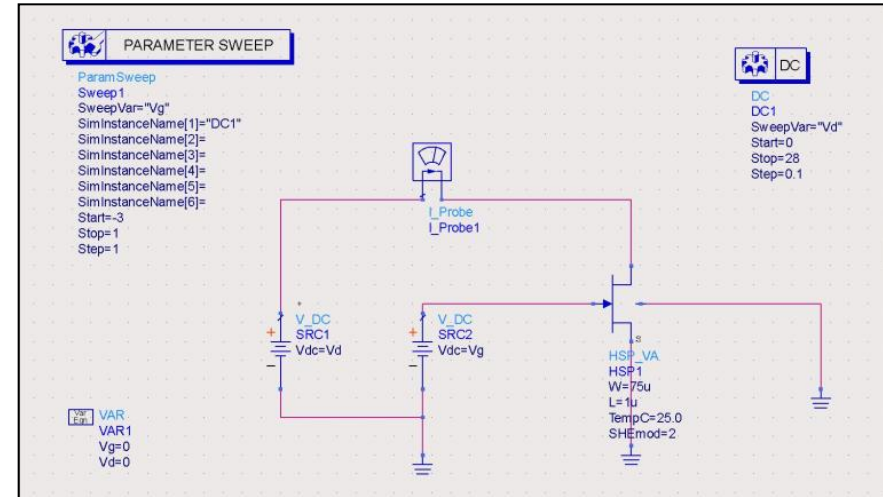
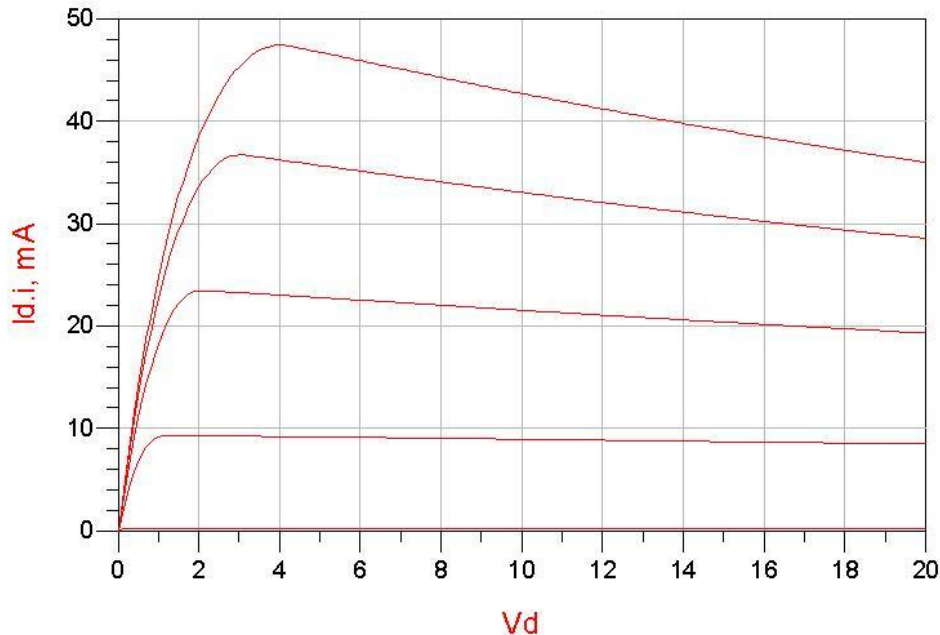


Experimental data from Wu'97



Verilog-A code + ADS simulation

L=1 μm and W=75 μm



Summary and conclusions

- **HSP: a new approach and attempt for power devices modeling**
- **Physical approach (temperature, Al content, band structure, SP & PZ polarizations, layer thicknesses, doping, incomplete donor activation, heat diffusion in substrate, ...)**
- **SP approach chosen for continuity of “inversion” charge**
- **Interesting tool for technological development (x_{Al} , Ga- or N-face, doping, layers thicknesses)**
- **This physical approach allows to estimate the impact of technological variations on electrical properties (variability)**
- **Further research efforts to improve the core model:
e.g. SHE algorithm convergence for very high temperature increase ($\Delta T > 300$ °C), Schottky gate current, impact of surface traps, ...**
- **Implementation using Verilog-A and ADS simulator from Agilent**

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**Many thanks to Luca Lucci
for fruitful discussions on power devices**

Thank you for your attention



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